### CS-184: Computer Graphics Lecture #20: Spring and Mass systems Prof. James O'Brien University of California, Berkeley Today Spring and Mass systems Distance springs Spring dampers Edge springs

	Hanging Cloth		
Huamin Wan Measureme BC Canada.	g, Ravi Ramamoorthi, and James F. O Biren: "Data-Driven Elastic Models for Cloth: Modeling and nt". ACM Transactions on Graphics, 30(4):71:1-11, July 2011. Proceedings of ACM SIGGRAPH 2011, Vancouver,	3	
	Walking Mannequin		
Huamin Wan <b>Measureme</b> BC Canada.	g, Ravi Ramamoothi, and James F. O'Brien. "Data-Driven Elastic Models for Cloth Modeling and art." ACM Transactions on Graphics, 30(q-71:1-11, July 2011. Proceedings of ACM SIGGRAPH 2011, Vancouver,	4	

### A Simple Spring

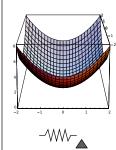
• Ideal **zero**-length spring

$$-$$
WW-  $f_{a \rightarrow b} = k_S(b - a)$ 

- $^*$  Force pulls points together  $oldsymbol{f}_{b 
  ightarrow a} = -oldsymbol{f}_{a 
  ightarrow b}$
- Strength proportional to distance

### A Simple Spring

• Energy potential



$$E = 1/2 k_s(\boldsymbol{b} - \boldsymbol{a}) \cdot (\boldsymbol{b} - \boldsymbol{a})$$

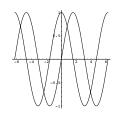
$$m{f}_{a o b} = k_S(m{b} - m{a})$$
 $m{f}_{b o a} = -m{f}_{a o b}$ 

$$f_{h \rightarrow a} = -f_{a \rightarrow b}$$

$$m{f}_a = -
abla_a E = -\left[rac{\partial E}{\partial a_x}, rac{\partial E}{\partial a_y}, rac{\partial E}{\partial a_z}
ight]$$

### A Simple Spring

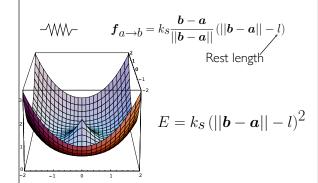
• Energy potential: kinetic **vs** elastic



$$E = 1/2 k_{\mathcal{S}}(\boldsymbol{b} - \boldsymbol{a}) \cdot (\boldsymbol{b} - \boldsymbol{a})$$

$$E = 1/2 \ m(\dot{\boldsymbol{b}} - \dot{\boldsymbol{a}}) \cdot (\dot{\boldsymbol{b}} - \dot{\boldsymbol{a}})$$

### Non-Zero Length Springs



## Comments on Springs • Springs with zero rest length are linear • Springs with non-zero rest length are nonliner • Force magnitude linear w/ discplacement (from rest length) • Force direction is non-linear • Singularity at $||\boldsymbol{b}-\boldsymbol{a}||=0$

### Damping

• "Mass proportional" damping

$$\stackrel{f}{\longleftarrow}$$

$$\boldsymbol{f} = -k_d \dot{\boldsymbol{a}}$$

- Behaves like viscous drag on all motion
- · Consider a pair of masses connected by a spring
- How to model rusty **vs** oiled spring
- Should internal damping slow group motion of the pair?
- Can help stability... up to a point

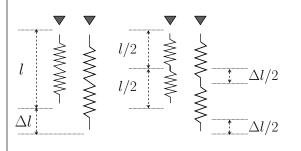
### Damping

"Stiffness proportional" damping

- · Consider a pair of masses connected by a spring
- How to model rusty vs oiled spring
- Should internal damping slow group motion of the pair?

### Spring Constants

• Two ways to model a single spring



20-SpringMassSystems.key - April 23, 2014

### Spring Constants

- $^{\star}$  Constant  $k_{\mathcal{S}}$  gives inconsistent results with different discretizations
- Change in length is not what we want to measure
- Strain: change in length as fraction of original length

$$\epsilon = \frac{\Delta l}{l_0} \quad \text{Nice and simple for ID...} \, , \label{epsilon}$$

### Structures from Springs • Sheets • Blocks

Others

### Structures from Springs They behave like what they are (obviously!) This structure will not resist shearing This structure will not resist outof-plane bending either... Structures from Springs They behave like what they are (obviously!) This structure will resist shearing but has anisotopic bias This structure still will not resist

out-of-plane bending

### Structures from Springs They behave like what they are (obviously!) This structure will resist shearing Interference between spring sets This structure still will not resist out-of-plane bending Structures from Springs They behave like what they are (obviously!) This structure will resist shearing Less bias Interference between spring sets This structure will resist out-ofplane bending Interference between spring sets

Odd behavior

How do we set spring constants?

### Edge Springs

$$u_{1} = |E| \frac{N_{1}}{|N_{1}|^{2}} \qquad u_{2} = |E| \frac{N_{2}}{|N_{2}|^{2}}$$

$$u_{3} = \frac{(x_{1} - x_{4}) \cdot E}{|E|} \frac{N_{1}}{|N_{1}|^{2}} + \frac{(x_{2} - x_{4}) \cdot E}{|E|} \frac{N_{2}}{|N_{2}|^{2}}$$

$$u_{4} = -\frac{(x_{1} - x_{3}) \cdot E}{|E|} \frac{N_{1}}{|N_{1}|^{2}} - \frac{(x_{2} - x_{3}) \cdot E}{|E|} \frac{N_{2}}{|N_{2}|^{2}}$$

$$F_{i}^{e} = k^{e} \frac{|E|^{2}}{|N_{1}| + |N_{2}|} \sin(\theta/2) u_{i}$$

From Bridson et al., 2003, also see Grinspun et al., 2003

### Example: Thin Material Discrete Shells SCA 2000 Ellan Grisqua, Anil Harari, Mathieu Destrun and Peter Schröder

# Strain Limiting Bunny Hollow Triangle Mesh 59K Elements Nacional College, per last Remonths, Valid-Bookfor burkey Research (Nacional Research Research (Nacional Research Re



Suggested Reading	
Physically Based Modeling: Principles and Practice Andy Witkin and David Baraff http://www-2.cs.cmu.edu/~baraff/sigcourse/index.html Grinspun, Hirani, Desbrun, and Peter Schroder, "Discrete Shells," SCA 2003 Bridson, Marino, and Fedkiw, "Simulation of Clothing with Folds and Wrinkles," SCA 2003 O'Brien and Hodgins, "Graphical Modeling and Animation of Brittle Fracture," SIGGRAPH 99	