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(54) **CAPACITIVE NON-CONTACT VOLTAGE SENSING METHOD AND APPARATUS**

(56) **References Cited**

U.S. PATENT DOCUMENTS

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4,723,220 A \* 2/1988 Smith-Vaniz ..... H02J 13/00034  
374/E1.019

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4,746,241 A \* 5/1988 Burbank, III ..... G01K 1/024  
374/E1.019

(Continued)

FOREIGN PATENT DOCUMENTS

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KR 1020140073457 A 6/2014  
TW 201947234 A 12/2019

OTHER PUBLICATIONS

(\*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

“FDC1004 4-Channel Capacitance-to-Digital Converter for Capacitive Sensing Solutions,” Texas Instruments Inc., FDC1004 SNOSCY5B, Aug. 2014, Revised Apr. 2015. www.ti.com.

(Continued)

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(57) **ABSTRACT**

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A non-contact electric potential meter system to determine voltage between an AC conductor and a reference potential without direct electrical contact to the conductor. A housing provides a shielded measurement region that excludes other conductors and holds power supply means; an AC voltage sensing mechanism includes a conductive sense plate and an electrical connection to the reference potential. Waveform-sensing electronic circuitry obtains an AC voltage waveform induced by capacitive coupling between the conductor and the conductive sense plate. Capacitance-determining electronic circuitry obtains a scaling factor based on the coupling capacitance formed between the conductor and the conductive sense plate. Signal processing electronic circuitry uses the AC voltage waveform and the coupling capacitance-based scaling factor to obtain the voltage between the conductor and the reference potential.

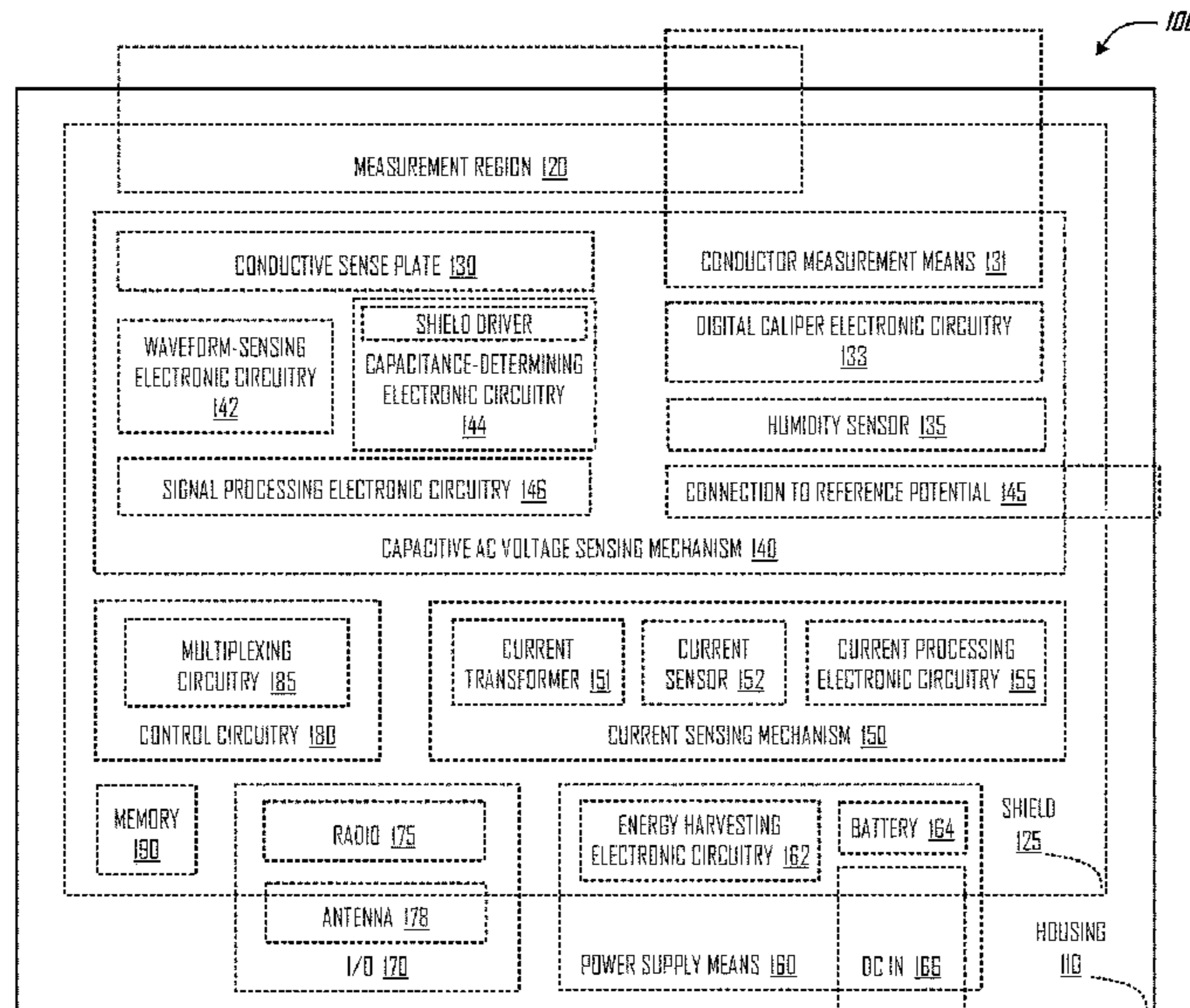
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See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

4,794,328	A *	12/1988	Fernandes .....	H02J 13/00002 374/E1.004
7,265,533	B2 *	9/2007	Lightbody .....	H05K 1/0268 324/126
9,322,854	B2	4/2016	Carpenter et al.	
9,347,976	B2 *	5/2016	Mason .....	G01R 15/16
10,352,967	B2	7/2019	Steuer et al.	
11,002,765	B1	5/2021	Lozek et al.	
11,209,480	B2 *	12/2021	Steuer .....	G01R 15/16
2012/0319675	A1	12/2012	El-Essawy et al.	
2013/0076343	A1	3/2013	Carpenter	
2015/0192618	A1	7/2015	Juds et al.	
2017/0227582	A1	8/2017	Iida et al.	
2018/0017602	A1	1/2018	Gavrilov et al.	
2018/0136257	A1	5/2018	Steuer et al.	
2018/0136263	A1	5/2018	Steuer et al.	
2020/0124643	A1	4/2020	Buhlmann et al.	

OTHER PUBLICATIONS

“New Fluke FieldSense Technology Enables Simultaneous Voltage and Current Measurements—Without Metallic Contact,” Fluke Corporation, 2017, pp. 1-3.  
“Programmable Touch Controller for Single Electrode Capacitance Sensors (Rev B),” Analog Devices Inc., Data Sheet AD7148, 2007-2015, pp. 1-56, Norwood Massachusetts. www.analog.com.  
“Single-Channel Capacitive Sensor for Touch or Proximity Detection with Shielded Sensing Electrode,” STMicroelectronics NV, Data Sheet STM8T141, Doc ID 15699 Rev 7, Jun. 2011, pp. 1-50. www.st.com.  
“Vizi Metering,” Vizi Systems Brochure—v0.3, revised on Oct. 21, 2021.  
Cleary, F., “Capacitive Touch Sensor Design Guide,” Microchip Technology Inc., Application Note AN2934, DS00002934B, 2020, pp. 1-48.  
Dutta, P., “Vizi Metering, Inc.: @ SkyView Ventures—Sep. 7, 2021,” Vizi Metering, Inc., Sep. 7, 2021, pp. 1-25.  
Ren, S. et al., “A Development of Capacitive Voltage Sensor for Non-Intrusive Energy Meter,” 15th International Conference on Electrical Engineering/Electronics, Computer, Telecommunications and Information Technology, IEEE, 2018, pp. 776-779.  
Wang, D., “Capacitive Sensing: Ins and Outs of Active Shielding,” Texas Instruments Inc., Application Report SNOA926A—Feb. 2015—Revised Feb. 2015, pp. 1-13. www.ti.com.  
Search Report received for Taiwanese Patent Application No. 110145179, dated Nov. 17, 2022, 1 page.

\* cited by examiner



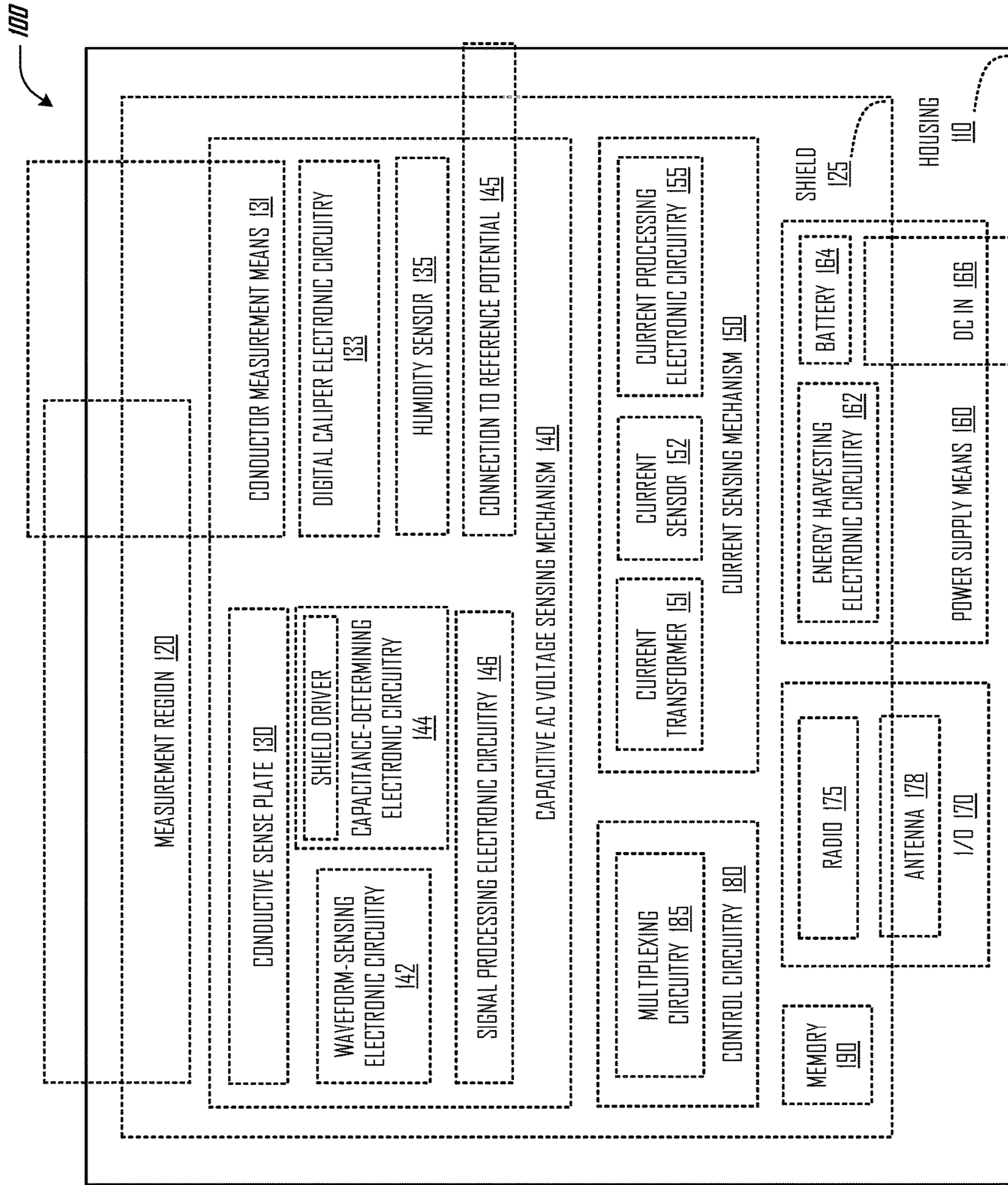
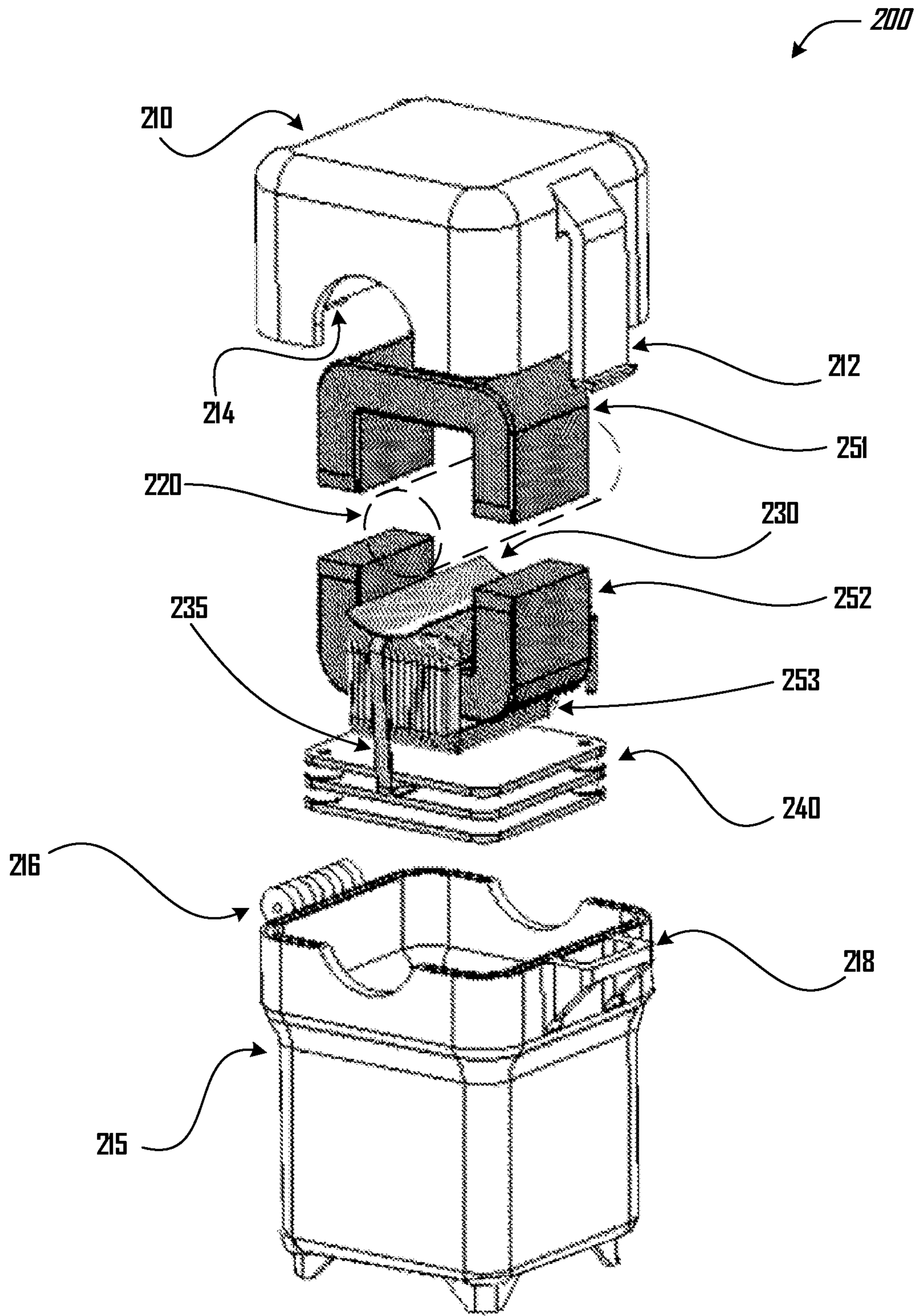
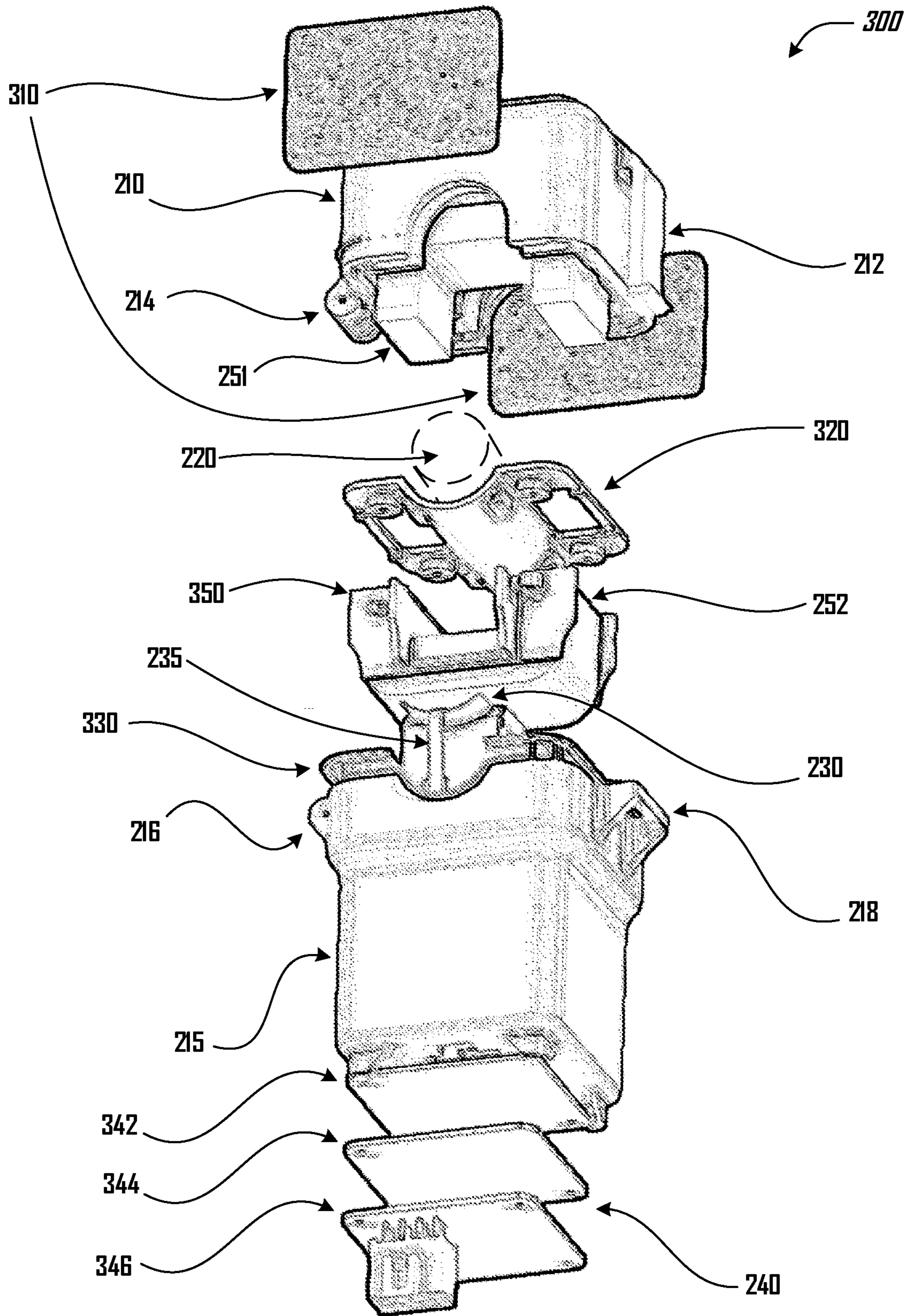


Fig. 1

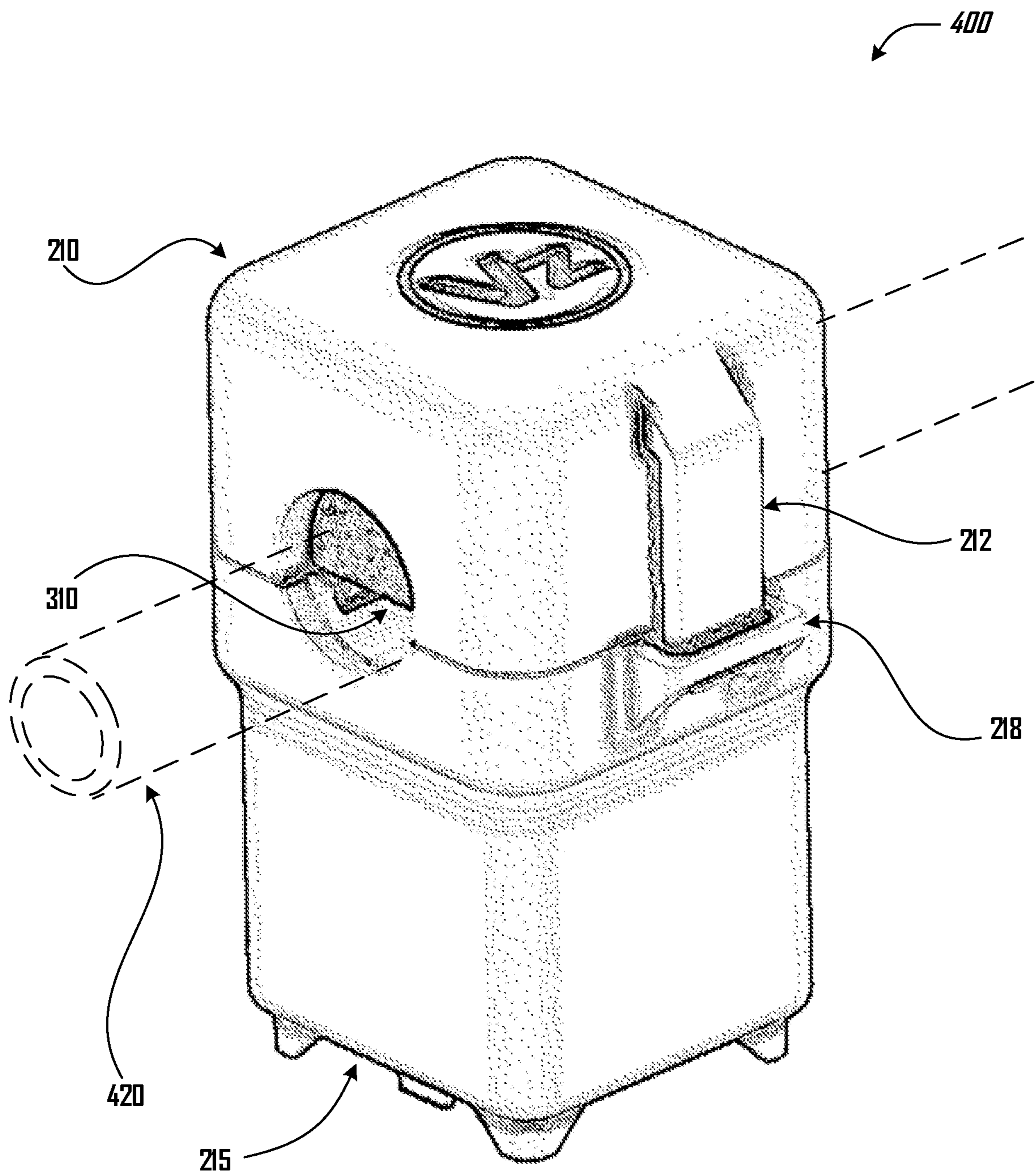


*Fig. 2*



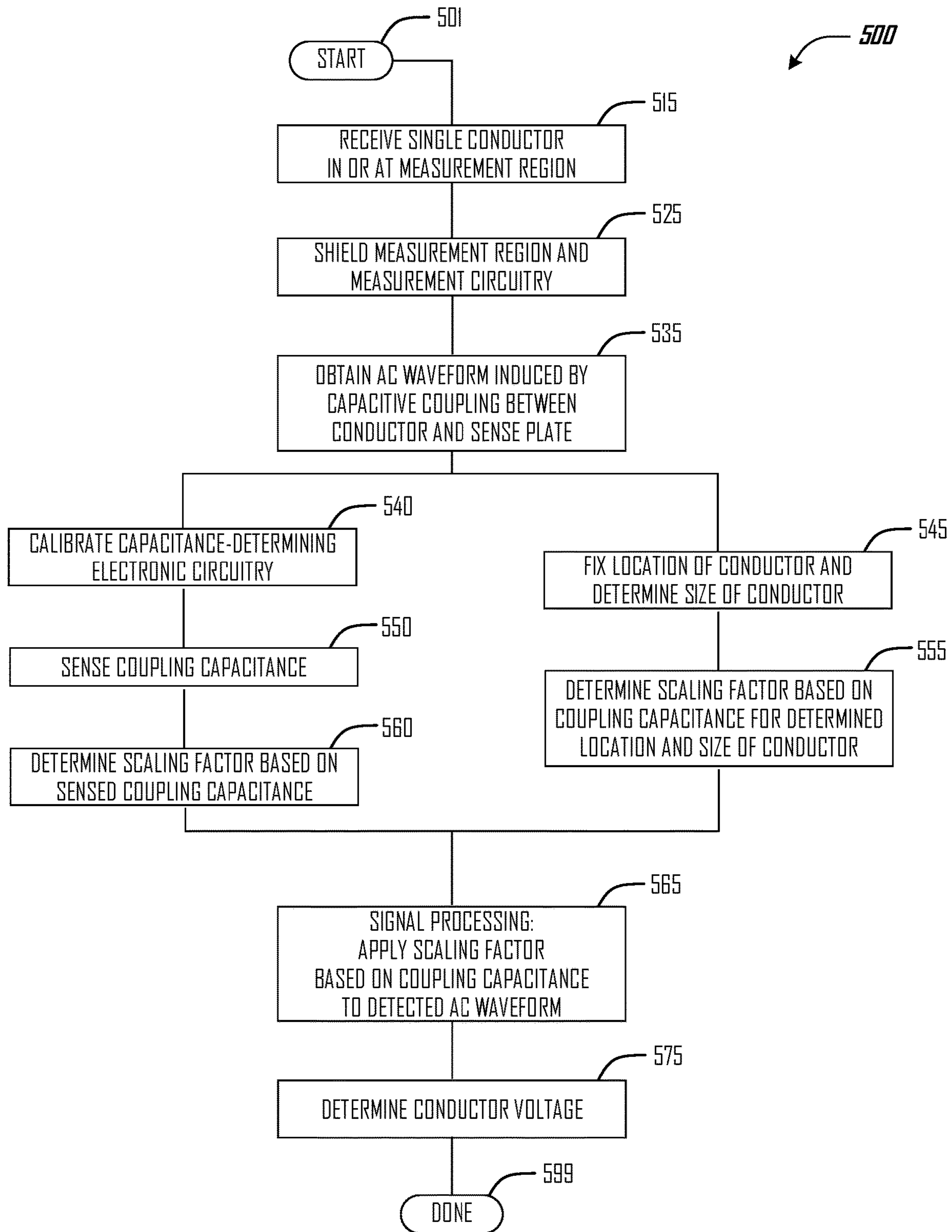


*Fig. 3*

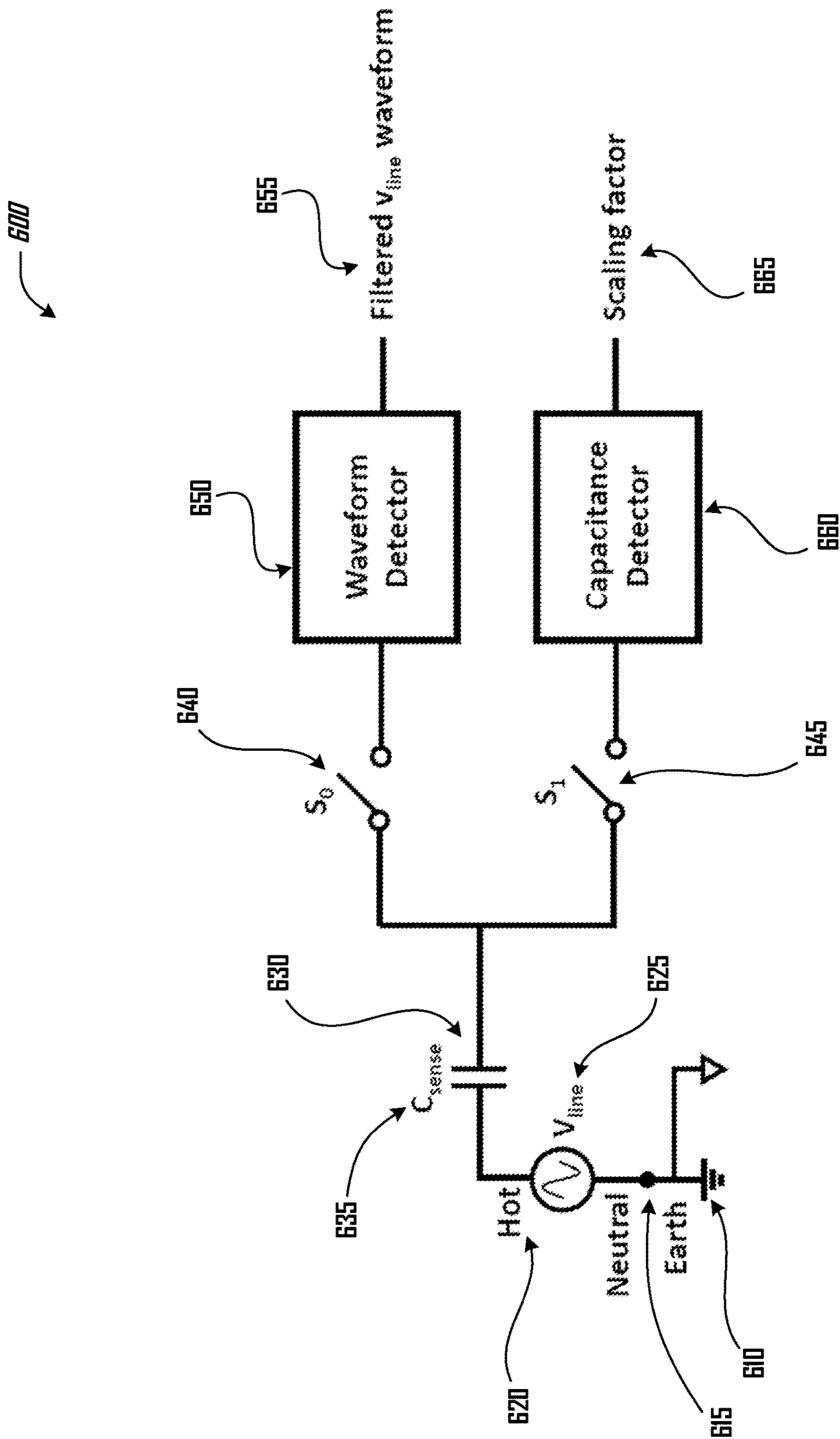


*Fig. 4*





*Fig. 5*



*Fig. 6*



700

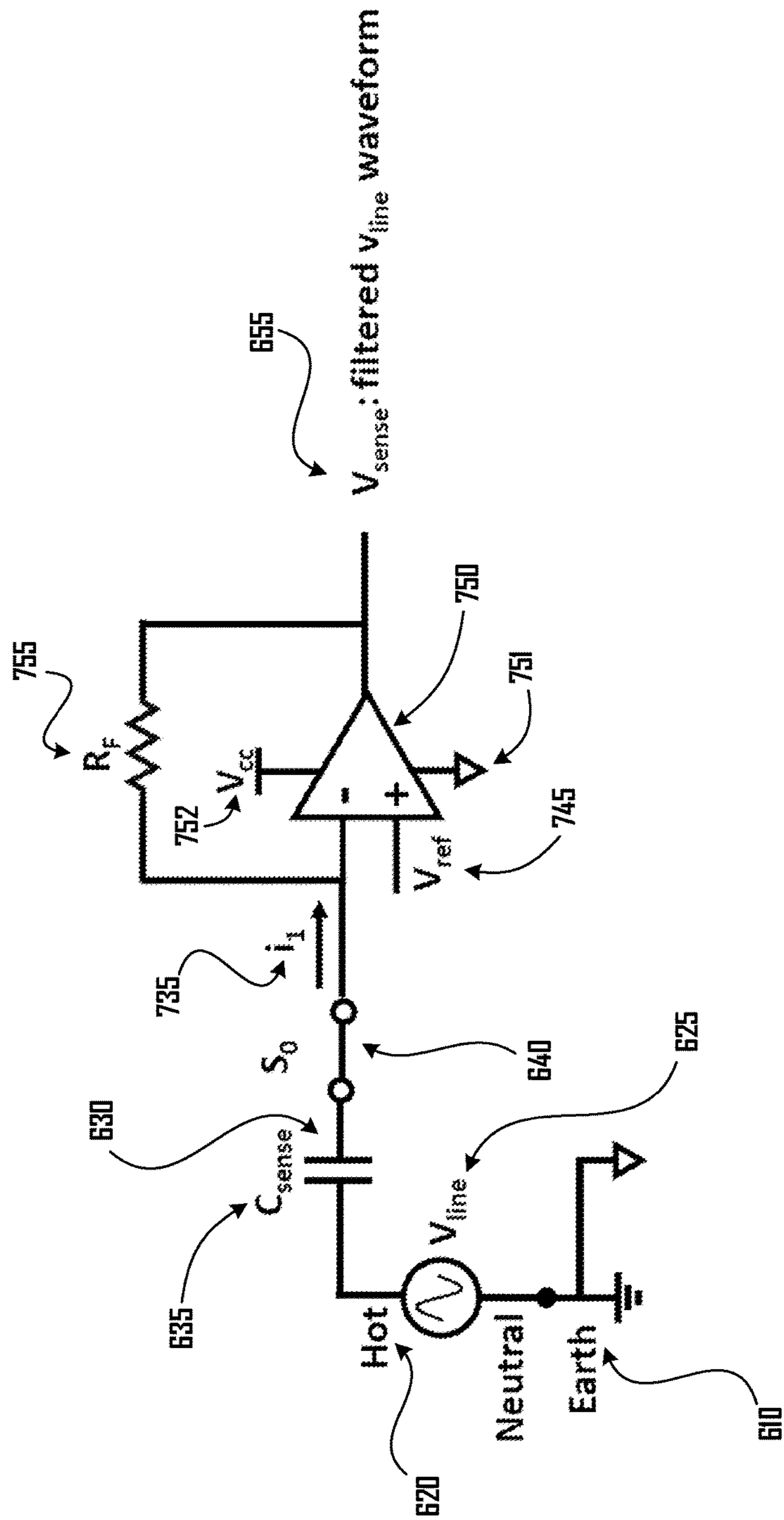
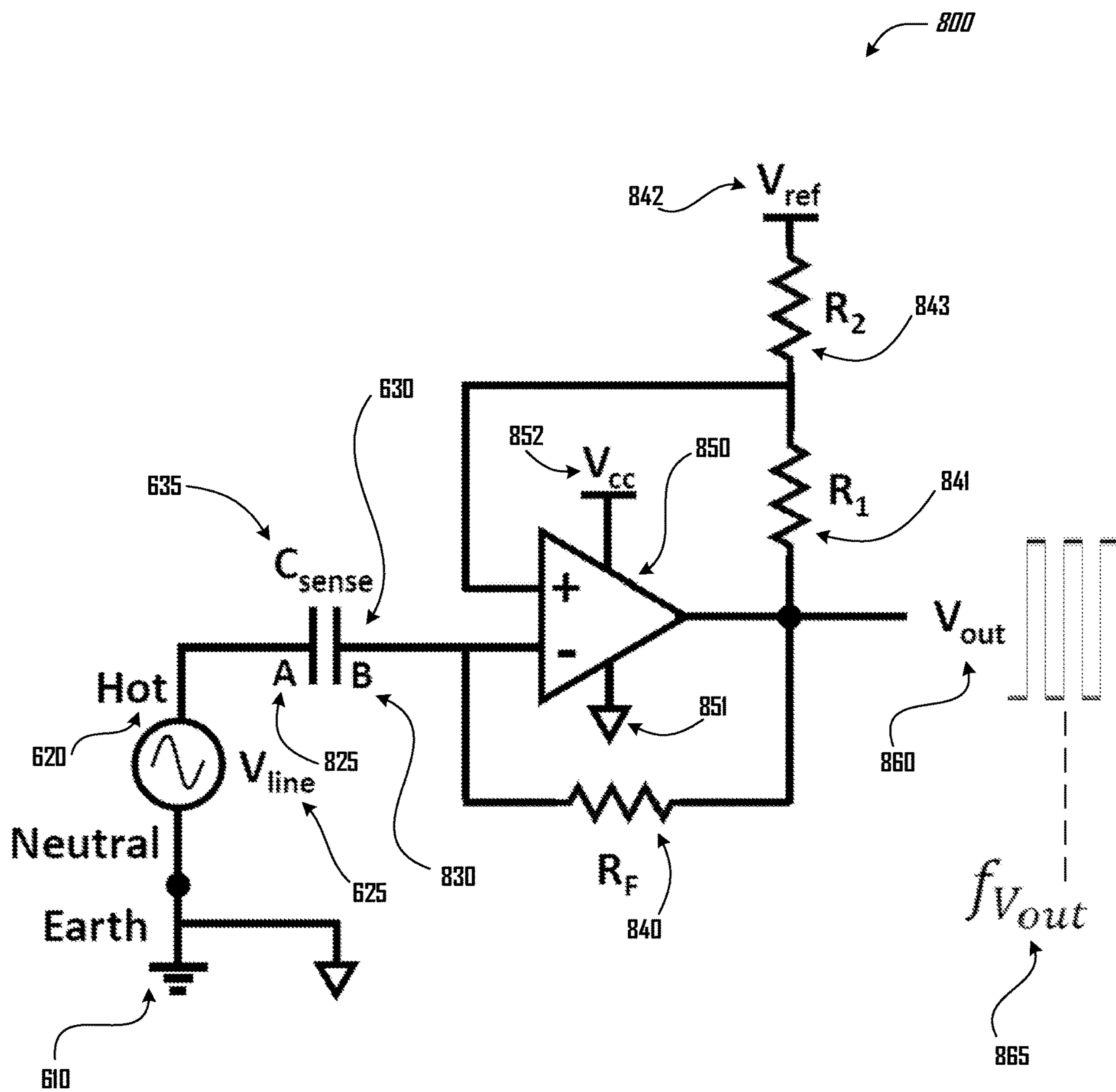


Fig. 7



*Fig. 8*

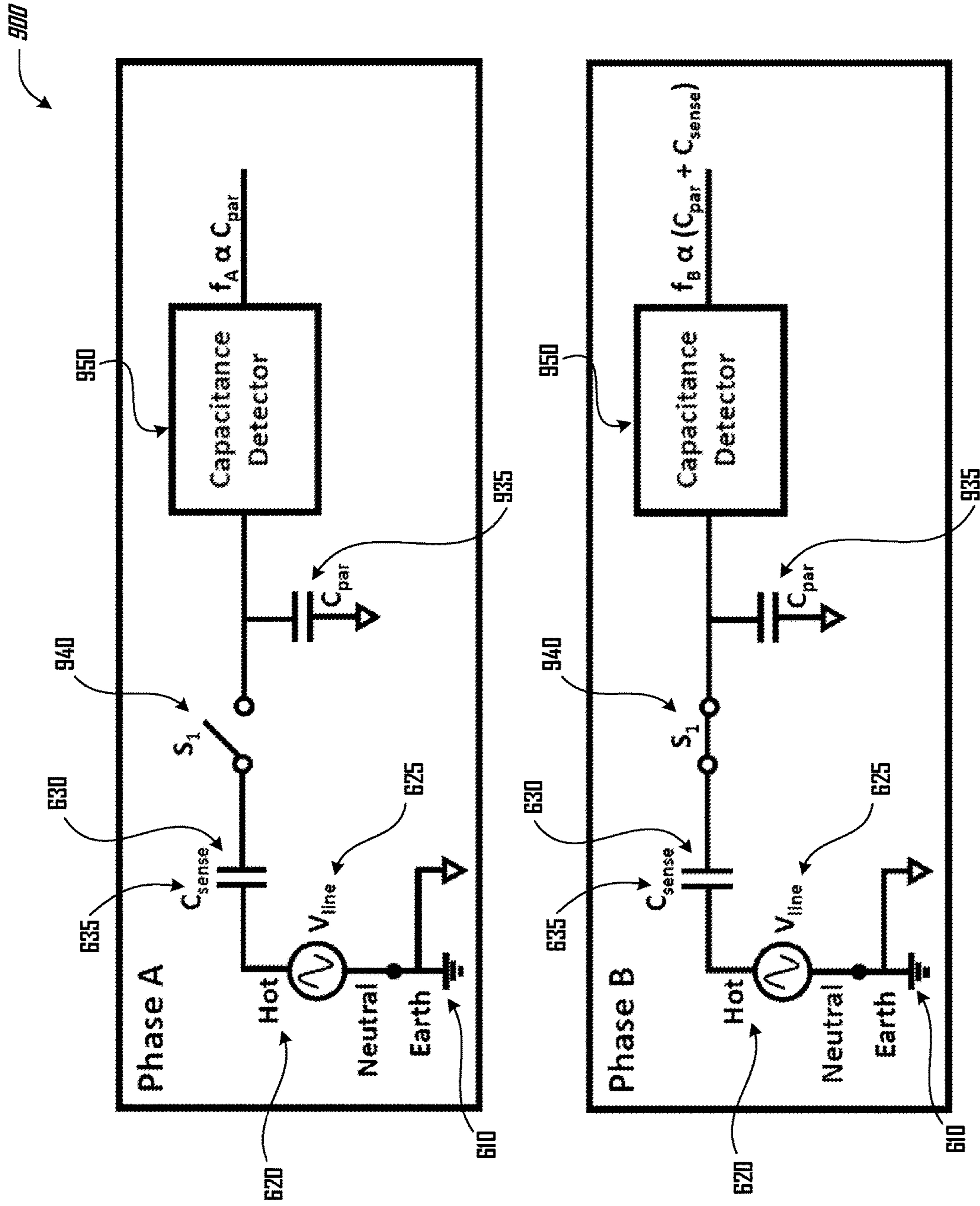
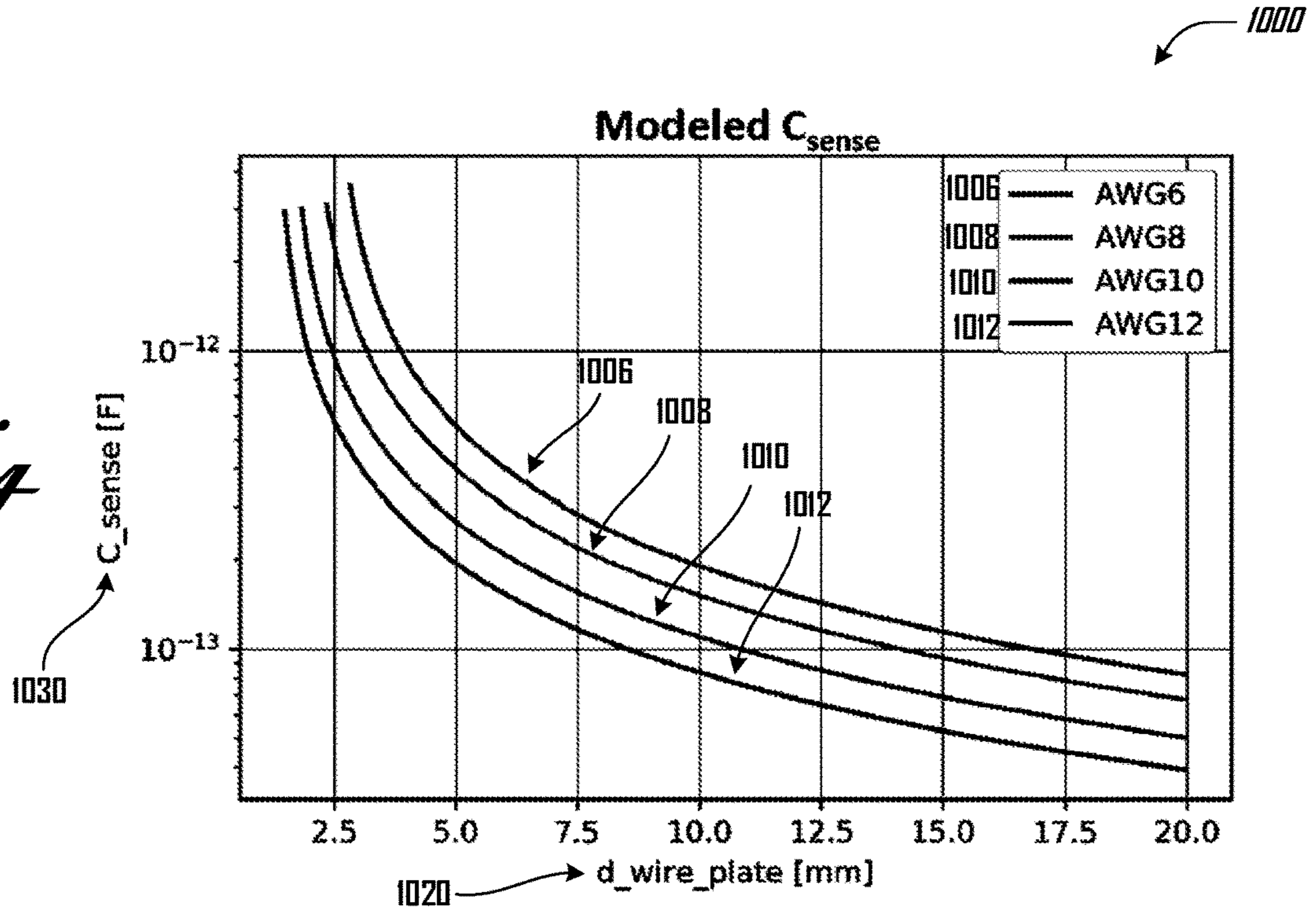


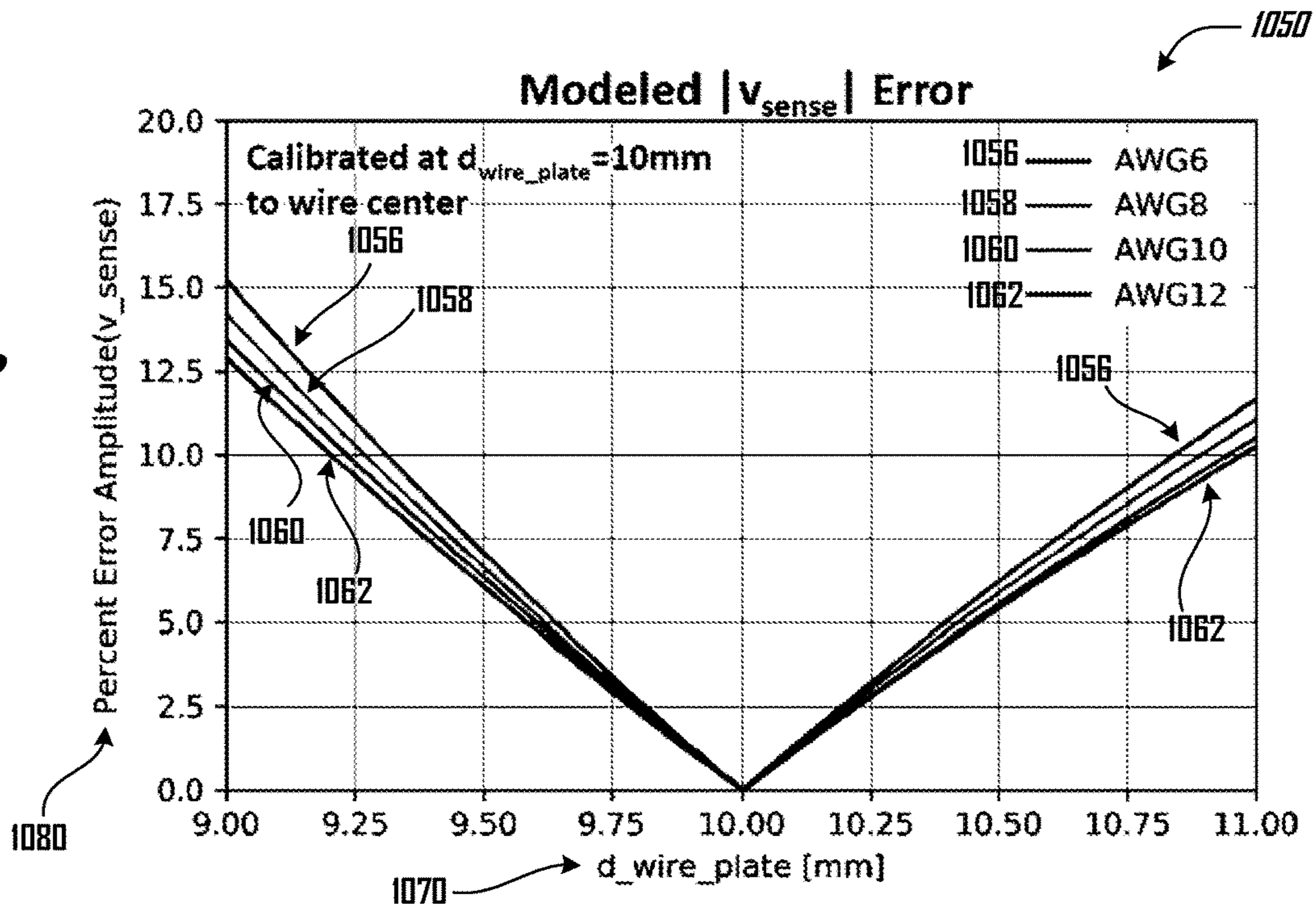
Fig. 9

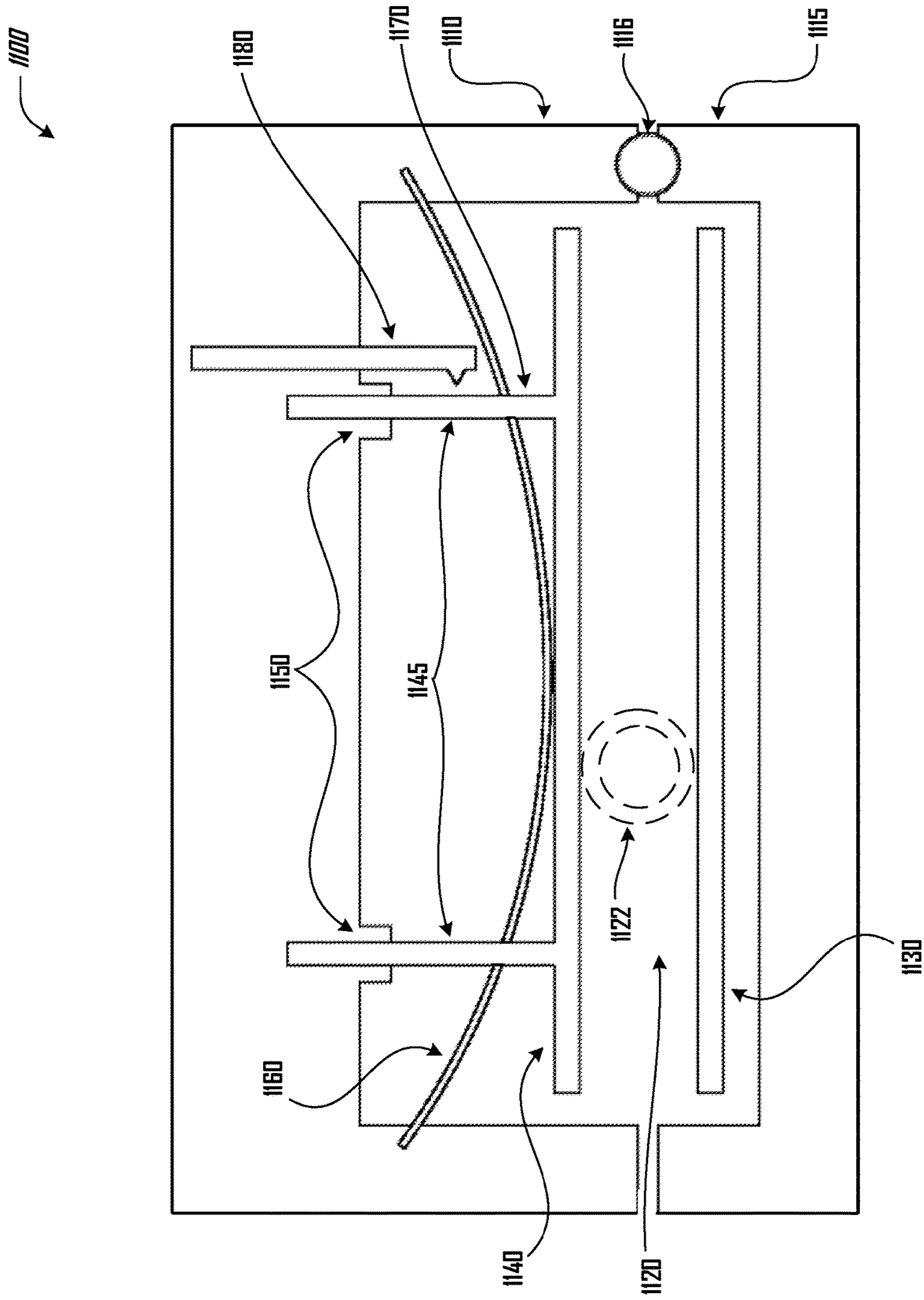


*Fig. 10A*

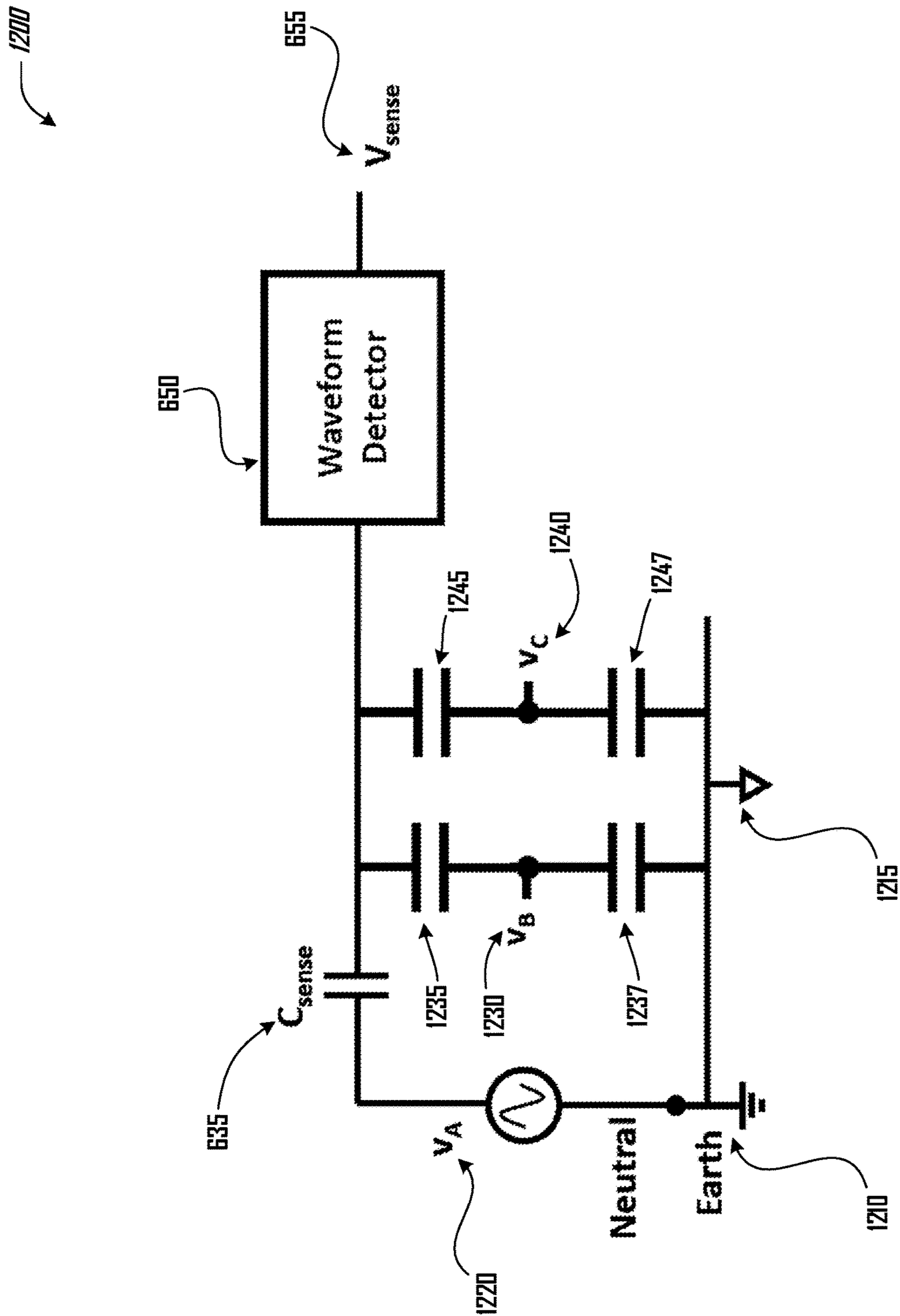


*Fig. 10B*



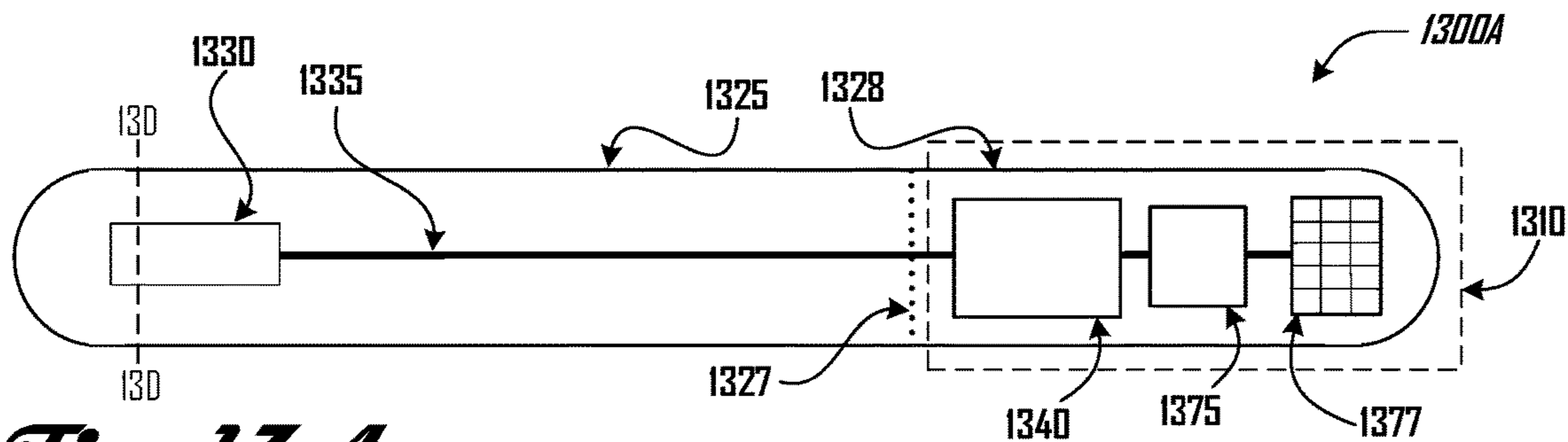


*Fig. 11*

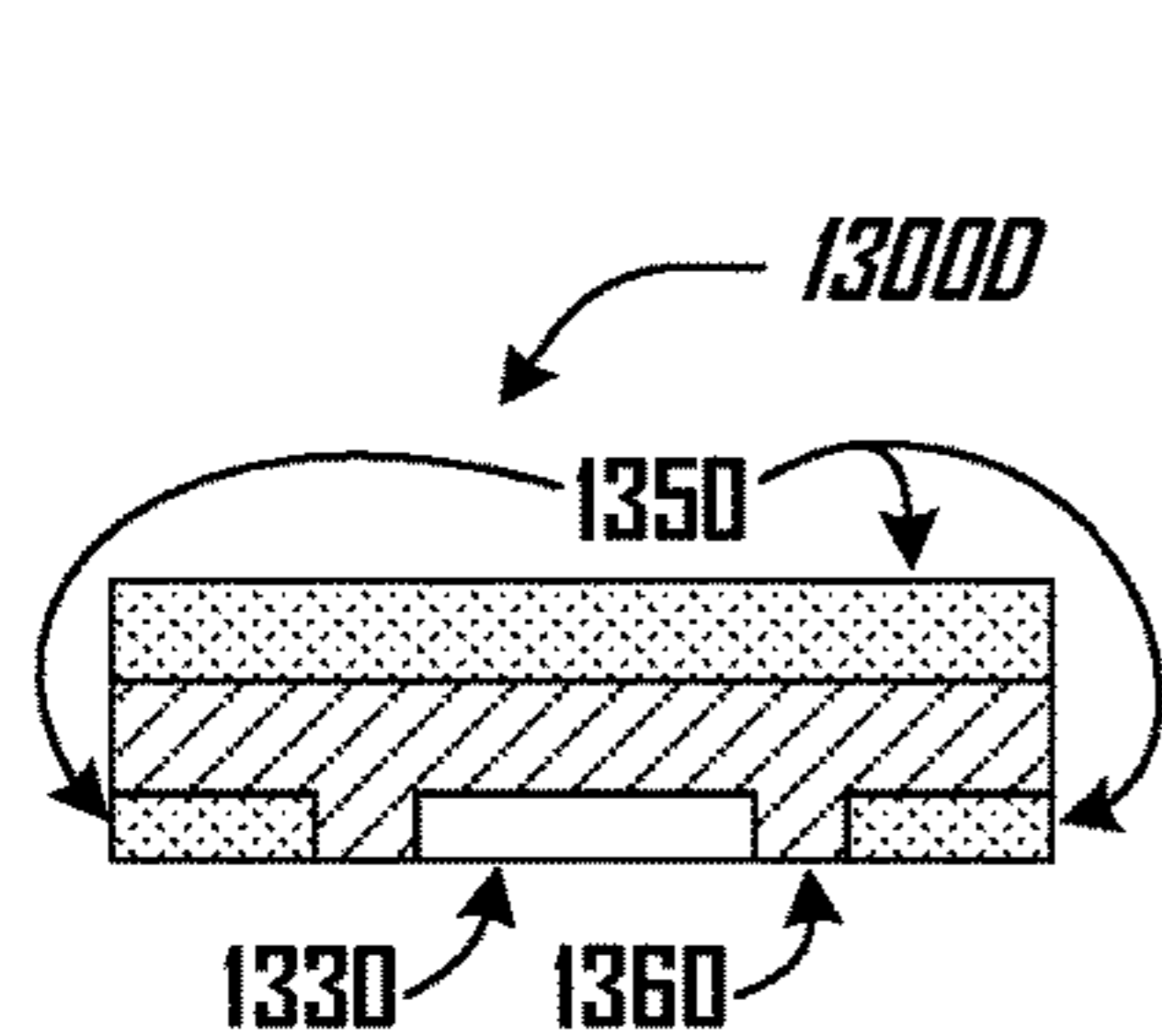


*Fig. 12*

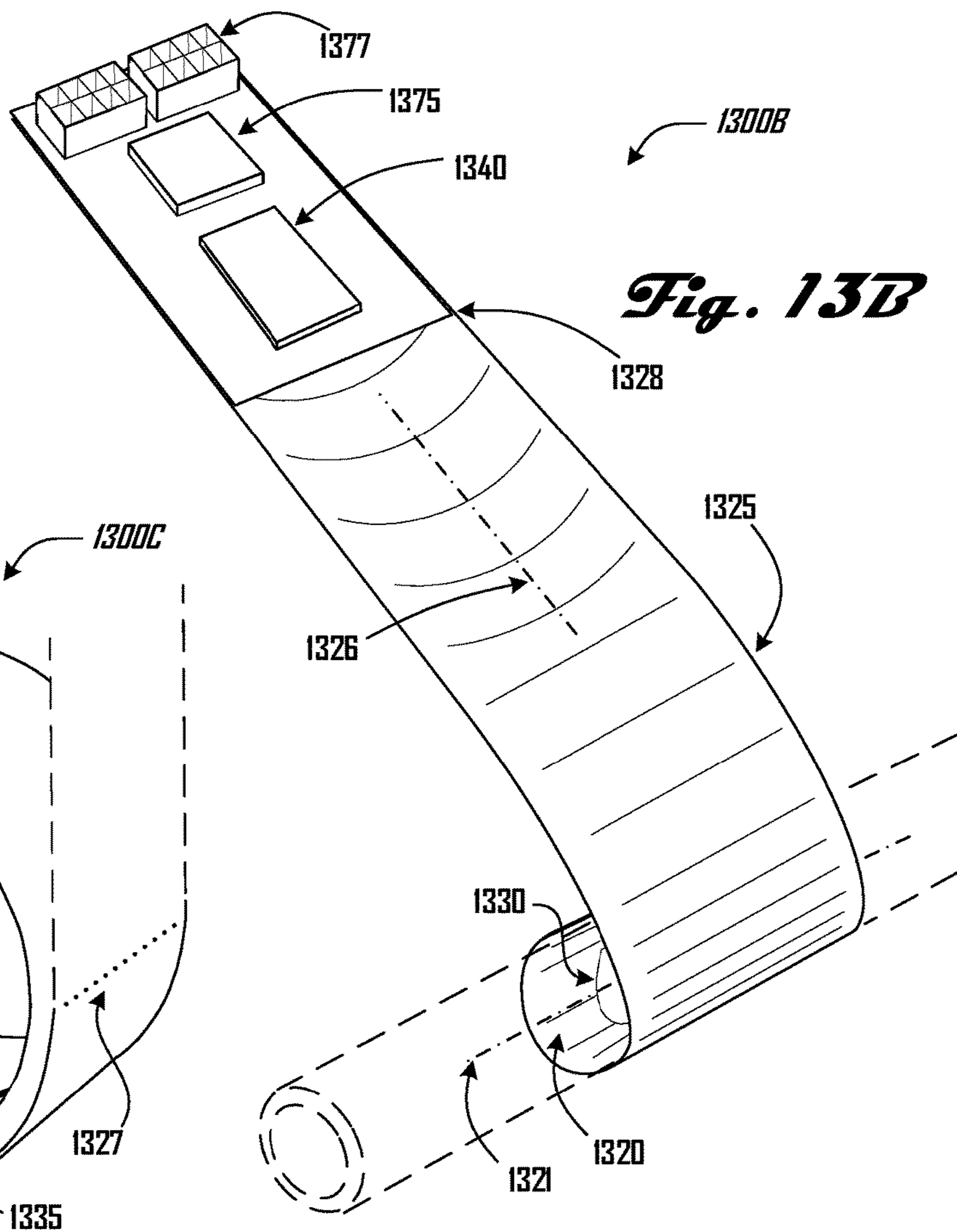




**Fig. 13A**



**Fig. 13D**



**Fig. 13B**

**Fig. 13C**



## CAPACITIVE NON-CONTACT VOLTAGE SENSING METHOD AND APPARATUS

### CROSS-REFERENCE TO RELATED APPLICATIONS

This application is a continuation-in-part of each of U.S. patent application Ser. No. 17/315,149, titled “NON-CONTACT VOLTAGE SENSING METHOD AND APPARATUS” and listing Michael C. Lorek as first inventor, filed May 7, 2021; which is a continuation of U.S. patent application Ser. No. 17/112,692, titled “NON-CONTACT VOLTAGE SENSING METHOD AND APPARATUS” and listing Michael C. Lorek as first inventor, filed Dec. 4, 2020, that issued as U.S. Pat. No. 11,002,765 on May 11, 2021. The entire contents of the above-referenced applications and of all priority documents referenced in the Application Data Sheet filed herewith are incorporated by reference herein, in their entireties, for all purposes.

### FIELD

This disclosure is directed to improved systems and methods of measuring electric potential in an alternating current (“AC”) conductor.

### BACKGROUND

Traditional approaches to measure AC voltage require making electrical contact with a target conductor and with a reference potential, forming a path with a voltmeter in parallel with the circuit to be measured.

### BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a block diagram illustrating operational components of an example non-contact voltage sensing apparatus in accordance with various embodiments.

FIG. 2 illustrates an exploded isometric view of components of an example non-contact voltage sensing apparatus in accordance with one embodiment.

FIG. 3 illustrates a different exploded breakout view of components of an example non-contact voltage sensing apparatus in accordance with one embodiment.

FIG. 4 illustrates a perspective view of an assembled example non-contact voltage sensing apparatus in accordance with one embodiment.

FIG. 5 illustrates an operational routine of a non-contact voltage sensing system in accordance with one embodiment.

FIG. 6 is a wiring diagram schematically illustrating a multiplexing circuit of electrical components configured to measure a waveform and a capacitance in accordance with one embodiment.

FIG. 7 is a wiring diagram schematically illustrating electrical components of a waveform detector circuit in accordance with one embodiment.

FIG. 8 is a wiring diagram schematically illustrating electrical components of a capacitance detector circuit in accordance with one embodiment.

FIG. 9 is a wiring diagram schematically illustrating electrical components of a calibration circuit configured to calibrate a capacitance detector circuit in accordance with one embodiment.

FIGS. 10A-10B are graphs illustrating a sensitivity of sensed capacitance to conductor size and distance from a conductive sense plate.

FIG. 11 illustrates physical components of an example conductor fixing and measurement system including a digital caliper in accordance with one embodiment.

FIG. 12 is a wiring diagram schematically illustrating multiphase coupling capacitances.

FIGS. 13A-13D illustrate schematic, perspective, and sectional views of example non-contact voltage sensing apparatuses having a flexible sensing attachment in accordance with various embodiments.

### DETAILED DESCRIPTION

This application discloses a non-contact electric potential meter system suitable for obtaining a determination of a voltage between a reference potential and an energized or “hot” conductor of an alternating current electrical circuit, without direct electrical contact to the first hot conductor and without comparison to any other AC voltage signal.

The technical advancements of the non-contact voltage sensing apparatus disclosed herein allow it to overcome the limitations of prior power meters and offer significant advantages over prior art electric voltage measuring devices. For example, the disclosed voltage sensing apparatus uses a non-contact capacitive coupling system and technique to measure the voltage signal in an AC conductor. This allows accurate voltage sensing—measurement of a properly shaped and scaled waveform, not just peak detection—without requiring physical contact to the hot conductor wire. The disclosed apparatus reduces installation time, does not require interruption of power, and detects harmonics in conductor voltages that can be used to detect and anticipate equipment failures or performance issues.

The disclosed technology obtains an AC waveform in a target energized conductor via capacitive coupling between the conductor and a sense plate that is situated near the conductor. An electronic circuit samples a waveform representing a filtered version of the AC voltage between the energized conductor and a reference potential. Another circuit determines the coupling capacitance between the conductor and the sense plate. Together, these allow analog or digital signal processing circuitry to recover the shape or frequency spectrum of the line voltage and to correctly scale the recovered waveform. Thus, the non-contact voltage sensing apparatus disclosed herein accurately determines the AC line voltage.

In addition, the disclosed technology allows a split-core current transformer (CT) to provide current measurements of the target conductor, and provides a multiplexing circuit to repurpose the current transformer (when it is not actively measuring current) as an energy harvester to supply runtime power for the non-contact voltage sensing apparatus. In some embodiments, a CT functions as a current sensor and energy harvester without multiplexing. For example, by estimation or calculation of energy harvester output voltage, current, or power, both energy harvesting and current sensing functions may be operated at the same time. Harvesting energy to power the non-contact voltage sensing apparatus and simultaneously measuring the current flowing in the target conductor can increase energy efficiency. For another example, components (such as energy harvesting electronic circuitry) may be turned off when current sensing circuitry is active.

Reference is now made in detail to the description of the embodiments as illustrated in the drawings. While embodiments are described in connection with the drawings and related descriptions, there is no intent to limit the scope to the embodiments disclosed herein. On the contrary, the



intent is to cover all alternatives, modifications, and equivalents. In alternate embodiments, additional sensing devices, or combinations of illustrated devices, may be added to, or combined, without limiting the scope to the embodiments disclosed herein. Each of the Figures discussed below may include many more or fewer components than those shown and described. Moreover, not all of the described components may be required to practice various embodiments, and variations in the arrangements and types of the components may be made. However, the components shown are sufficient to disclose various illustrative embodiments for practicing the disclosed technology.

The embodiments set forth below are primarily described in the context of measuring electric circuits such as residential, commercial, industrial, or utility-level wiring (including, e.g., power transmission and distribution networks). However, the embodiments described herein are illustrative examples and in no way limit the disclosed technology to any particular size, construction, or application of conductor.

The phrases “in one embodiment,” “in various embodiments,” “in some embodiments,” and the like are used repeatedly. Such phrases do not necessarily refer to the same embodiment. The terms “comprising,” “having,” and “including” are synonymous, unless the context dictates otherwise. As used in this specification and the appended claims, the singular forms “a,” “an,” and “the” include plural referents unless the content clearly dictates otherwise. For example, “a scaling factor” generally includes multiple scaling factors. It should also be noted that the term “or” is generally employed in its sense including “and/or” unless the content clearly dictates otherwise.

The terms “sense”/“sensing,” “meter”/“metering,” “detect”/“detecting,” and “measure”/“measuring” are generally synonymous, unless the context dictates otherwise. For example, “detecting” an AC waveform generally refers to obtaining measurement of a continuously varying alternating current, and not only obtaining a Boolean value representing whether an AC waveform is present. A “detector” likewise should be interpreted as a device to obtain measurements and not only to detect presence. The terms “electric” and “electrical” are generally synonymous. The terms “voltage” and “potential” or “electric(al) potential” are also generally synonymous. Similarly, the terms “amperage” and “current” or “electric(al) current” are generally synonymous. Thus, the terms “voltage sensing apparatus” and “electric potential meter system” are used synonymously.

The disclosed non-contact voltage sensing apparatus can take a variety of form factors. FIGS. 1 through 13 illustrate a variety of different arrangements, designs, and subsystem possibilities. The illustrated sensing systems and methods are not an exhaustive list; in other embodiments, a measurement region for receiving a conductor or circuitry for powering and/or controlling a non-contact voltage sensing apparatus could be formed in different arrangements. However, it is not necessary to exhaustively show such optional implementation details to describe illustrative embodiments.

FIG. 1 is a block diagram illustrating operational components of an example non-contact voltage sensing apparatus 100 in accordance with one embodiment. The apparatus 100 typically includes a housing 110. The apparatus 100 includes a measurement region 120 that is configured to receive a conductor, e.g., a “hot” AC conductor (or “line”) such as an insulated copper wire. The non-contact voltage sensing apparatus 100 is configured so that when the measurement region 120 receives the conductor, the conductor is not interrupted. In various embodiments, the measurement

region 120 in operation receives a single conductor, and is configured to exclude other conductors (including, e.g., any additional “hot” wire). In various embodiments, the housing 110 provides, defines, or indicates the measurement region 120. In various embodiments, the measurement region 120 is configured such that the conductor passes along, into, or through the measurement region 120. Thus, the measurement region 120 may be arranged inside and/or outside the housing 110.

The non-contact voltage sensing apparatus 100 further includes a shield 125. The shield 125 may be constructed of material having high conductivity, such as a metallic foil or mesh. In various embodiments, the shield 125 may form a Faraday cage around a portion or all of the components of the non-contact voltage sensing apparatus 100, such as around the measurement circuitry and conductive sense plate described below with respect to this FIG. 1. In some embodiments, the shield 125 may extend only partly around a portion or all of the components of the non-contact voltage sensing apparatus 100, and/or may include one or more apertures, e.g., to accommodate a conductor in the measurement region 120. In some embodiments, the shield 125 does not surround the measurement region 120. In some embodiments, the shield 125 is connected or connectable to a ground or neutral potential. In some embodiments, the shield 125 is actively driven to a reference potential or to a potential to match that of an electrode or conductive sense plate.

The illustrated non-contact voltage sensing apparatus 100 includes a capacitive AC voltage sensing mechanism 140. The voltage sensing mechanism 140 includes components configured to obtain a determination of an AC voltage in a conductor in the measurement region 120, such as by sensing an AC line voltage waveform, determining a scaling factor based on coupling capacitance, and processing the waveform and the scaling factor as further described in this disclosure.

The capacitive AC voltage sensing mechanism 140 includes an electrode or conductive sense plate 130 configured so that the conductive sense plate 130 forms a capacitive coupling with a conductor in the measurement region 120. The non-contact voltage sensing apparatus 100 further includes an electrical connection connectable to a reference potential 145, used in determining a voltage between the conductor and the reference potential. The electrical connection to a reference potential 145 may include a resistive or capacitive connection to a ground potential. In some embodiments, the non-contact voltage sensing apparatus 100 drives the electrical connection to the reference potential 145. For example, actively driving the shield 125 and the conductive sense plate 130 with the same signal, or driving the shield 125 to match a voltage of the conductive sense plate 130, can reduce the effects of parasitic capacitances to facilitate more accurate measurement of a voltage in a target conductor.

In various embodiments, the non-contact voltage sensing apparatus 100 is configured so that the conductive sense plate 130 has a determined or otherwise determinable geometric relationship to the conductor when the measurement region 120 receives the conductor. The geometric relationship between the conductor and the conductive sense plate 130, and, e.g., the size or other physical characteristics of the conductor (such as a wire gauge and/or insulation jacket thickness) may be known, fixed, or pre-set; or they may be measurable or similarly determinable. In some embodiments, the non-contact voltage sensing apparatus 100 is configured to automatically position the conductive sense



5

plate **130** and/or the conductor with respect to one another. Illustrative examples of various such configurations are described in further detail with reference to FIG. **3**, FIG. **11**, and FIGS. **13A-C** below. In some embodiments, the non-contact voltage sensing apparatus **100** includes conductor measurement means **131** to fix and/or measure one or more aspects of the conductor at the measurement region **120**. An example conductor measurement means **131** and digital caliper electronic circuitry **133** is described in further detail with reference to FIG. **11** below. In some embodiments, the non-contact voltage sensing apparatus **100** includes a humidity sensor **135**, so that the apparatus **100** can identify and compensate for changes in the dielectric constant of air associated with changes in humidity.

The capacitive AC voltage sensing mechanism **140** includes waveform-sensing electronic circuitry **142** configured to sense an AC line voltage waveform. The waveform-sensing electronic circuitry **142** may obtain the AC waveform by measuring a current induced via capacitive coupling between the sense plate **130** and an energized conductor in the measurement region **120**. The waveform-sensing electronic circuitry **142** may include an operational amplifier (“op-amp”) circuit, such as described in further detail with reference to FIG. **7** below.

The capacitive AC voltage sensing mechanism **140** further includes capacitance-determining electronic circuitry **144** (also referred to herein as coupling capacitance tracking electronic circuitry) configured to sense a coupling capacitance between the conductive sense plate **130** and the conductor in the measurement region **120**. In some embodiments, the capacitance-determining electronic circuitry **144** includes elements having an output frequency that depends in part on the coupling capacitance, such as described in further detail with reference to FIG. **8** below. In some embodiments, the capacitance-determining electronic circuitry **144** includes an active signal driver that drives the conductive sense plate **130** and/or the shield **125**.

In some embodiments, the active signal driver is a capacitance measurement chip or circuit with active or driven shield functionality, such as used in non-analogous contexts to, for example, sense the presence of a finger pressing a capacitive sensing button. Examples of such capacitance measurement chips include a Texas Instruments® (“TI”) FDC1004 capacitance to digital converter microchip; a Microchip Technology MTCH1010 touch controller microchip; an Analog Devices, Inc. AD7148 capacitive touch controller chip; and an ST Microelectronics STM8T141 capacitive sensor package. The contents of the TI FDC1004 datasheet titled “FDC1004 4-Channel Capacitance-to-Digital Converter for Capacitive Sensing Solutions” and of the TI Application Report titled “Capacitive Sensing: Ins and Outs of Active Shielding”; the contents of the Microchip Technology MTCH1010 datasheet titled “MTCH1010 Data Sheet” and of the Microchip Application Note AN2934 titled “Capacitive Touch Sensor Design Guide”; the contents of the Analog Devices AD7148 datasheet titled “Programmable Touch Controller for Single Electrode Capacitance Sensors (Rev. B)” and the contents of the ST Microelectronics STM8T141 datasheet titled “Single-channel capacitive sensor for touch or proximity detection with shielded sensing electrode” are each incorporated by reference herein. Such a capacitance measurement chip or circuit may be configured to drive the conductive sense plate **130** and/or the shield **125** with a high frequency (e.g., approximately 25 kHz) waveform.

The capacitive AC voltage sensing mechanism **140** further includes signal processing electronic circuitry **146**. The

6

signal processing electronic circuitry **146** processes the AC line voltage waveform representation obtained by the waveform-sensing electronic circuitry **142** to recover a shape or frequency spectrum of the line voltage waveform. The signal processing electronic circuitry **146** may process the coupling capacitance determination obtained by the capacitance-determining electronic circuitry **144** to obtain a scaling factor. The signal processing electronic circuitry **146** may also use the determination of one or more physical characteristics of the conductor obtained by the conductor measurement means **131** (e.g., via the digital caliper electronic circuitry **133**) to obtain a scaling factor. The signal processing electronic circuitry **146** scales the recovered shape or frequency spectrum of the line voltage waveform according to the scaling factor(s) to obtain an accurate measurement of the true AC line voltage in the conductor in the measurement region **120**. In various embodiments, the signal processing electronic circuitry **146** may include analog and/or digital signal processing components.

In some embodiments, the non-contact voltage sensing apparatus **100** includes a current sensing mechanism **150**. The current sensing mechanism **150** may include a current transformer (“CT”) **151**, a current sensor **152**, and current processing electronic circuitry **155**. The current sensor **152** may be a split-core current transformer, a solid-core current transformer, a Rogowski coil, an anisotropic magnetoresistance (AMR) sensor, a giant magnetoresistance (GMR) sensor, a Hall effect sensor, a current-sensing resistor, an inductor, etc. In some embodiments, the signal processing electronic circuitry **146** can process and time-synchronize a current waveform and a voltage waveform to obtain a determination of a power factor based on the detected AC electric current and voltage.

In various embodiments, the non-contact voltage sensing apparatus **100** includes power supply means **160** configured to power the electronic circuitry of the non-contact voltage sensing apparatus **100**. For example, the power supply means **160** may include a stored energy system such as a capacitor or battery **164**; an external power supply such as a direct current (“DC”) voltage source **166**; or means for obtaining energy from an AC conductor, such as energy harvesting electronic circuitry **162**. For example, the power supply means **160** may be configured to obtain power from the conductor via the measurement region **120**, e.g., via the current transformer **151** of the current sensing mechanism **150**.

In various embodiments, the non-contact voltage sensing apparatus **100** includes control circuitry **180**. The control circuitry **180** may include multiplexing circuitry **185** configured to share or switch components among or between circuits. For example, the control circuitry **180** may multiplex **185** the conductive sense plate **130** between the waveform-sensing electronic circuitry **142** and the capacitance-determining electronic circuitry **144**. As another example, the control circuitry **180** may multiplex **185** the current transformer **151** between the current sensing mechanism **150** and the energy harvesting electronic circuitry **162**. As yet another example, the control circuitry **180** may multiplex **185** the shield **125** between the electrical connection to the reference potential **145** (e.g., when the waveform-sensing electronic circuitry **142** is in operation) and the conductive sense plate **130** (e.g., for electrical driver circuitry to drive them to the same potential, minimizing a difference in potential between them and thus minimizing a displacement current, thereby minimizing effects of capacitance between them or hiding them from the measurement circuit when the capacitance-determining electronic circuitry **144** is in opera-



tion). The multiplexing circuitry **185** may reconfigure sub-circuits to include or exclude components such that they can perform multiple functions without interfering with one another. The multiplexing circuitry **185** may operate according to various algorithms based on time (e.g., at even, 5 uneven, or irregular intervals or according to a schedule), need (e.g., based on one or more signals received by the control circuitry **180**, such as a battery **164** level), sensed voltage and/or current values, or other factors.

In addition, the control circuitry **180** may be configured to 10 combine properly scaled sampled waveforms measured by the voltage sensing mechanism **140** (e.g., by the waveform-sensing electronic circuitry **142**, scaled according to the capacitance-determining electronic circuitry **144**) with current measurements obtained by the current sensing mechanism **150**, allowing the non-contact voltage sensing apparatus **100** to calculate a power dissipation, power delivery, or power factor, among other possible calculations including real, reactive, and apparent power.

In various embodiments, a data bus connects the various 20 internal systems and logical components of the non-contact voltage sensing apparatus **100**. For example, the control circuitry **180** may include circuitry to cause measurements to be recorded to memory **190** and/or transmitted via input/output (“I/O”) components **170** such as a radio **175** transceiver (e.g., with antenna **178**) for transmitting and/or receiving radio frequency (“RF”) signals (e.g., via low-power wide-area network (“LPWAN”) [e.g., LoRa, Sigfox, LTE-M, NB-IoT, etc.], Bluetooth, Wi-Fi, ZigBee, cellular network connection, NFC, RFID, etc.) or other interface 25 (e.g., a wired communication port such as USB, UART, etc.). The I/O components **170** may allow data (including, e.g., recorded voltage measurements) to be sent from the non-contact voltage sensing apparatus **100** to an external device or destination. The I/O components **170** may also allow instructions to be transmitted to the control circuitry **180** or other components of the non-contact voltage sensing apparatus **100** such as the memory **190**. The I/O components **170** may interface with, e.g., specialized meter reading devices, mobile phones, desktop computers, laptops, tablets, 30 wearable computers, or other computing devices that are configured to connect to the non-contact voltage sensing apparatus **100**.

The memory **190** can include a combination of temporary and/or permanent storage, and both read-only memory (“ROM”) and writable memory (e.g., random access memory (“RAM”), processor registers, and on-chip cache memories), writable non-volatile memory such as flash memory or other solid-state memory, hard drives, removable media, magnetically or optically readable discs and/or tapes, 35 nanotechnology memory, synthetic biological memory, and so forth. A memory is not a propagating signal divorced from underlying hardware; thus, a memory and a computer-readable storage medium do not refer to a transitory propagating signal per se. The memory **190** includes data storage that contains programs, software, and/or information, such as an operating system (e.g., an embedded real-time operating system), application programs or functional routines, and data (e.g., data structures, database entries, waveform representations, measurement records, calculation results, etc.).

The non-contact voltage sensing apparatus **100** may include a subset or superset of the components described above. Additional components may include, e.g., a display screen (such as an LCD, LED, or OLED display screen or an e-ink display), a speaker for playing audio signals, a 40 haptic feedback device for tactile output such as vibration,

etc., an environmental sensor such as a temperature sensor, power managing or regulating systems, etc. In various embodiments, additional infrastructure as well as additional devices may be present. Further, in some embodiments, the 5 functions described as being provided by some or all of the non-contact voltage sensing apparatus **100** may be implemented via various combinations of physical and/or logical devices, e.g., one or more replicated and/or distributed physical or logical devices. For example, in some embodiments, the non-contact voltage sensing apparatus **100** includes a sensor configured to capture and wirelessly transmit voltage parameters (shape, frequency components and phases, etc.) to an external device, and may or may not include any current sensing or signal processing circuitry.

Aspects of the non-contact voltage sensing apparatus **100** can be embodied in a specialized or special purpose computing device or data processor that is specifically programmed, configured, or constructed to perform one or more of the computer-executable instructions explained in detail 15 herein. For example, the control circuitry **180** can be embodied in a microcontroller or an application-specific integrated circuit (“ASIC”). Various circuits or circuitry of the non-contact voltage sensing apparatus **100** may include or be embodied in a processing component that controls operation of the non-contact voltage sensing apparatus **100** in accordance with computer-readable instructions stored in memory **190**. A processing component may be any logic processing unit, such as one or more central processing units (“CPUs”), graphics processing units (“GPUs”), digital signal processors (“DSPs”), field-programmable gate arrays (“FPGAs”), ASICs, etc. A processing component may be a single processing unit or multiple processing units in an electronic device or distributed across multiple devices. Aspects of the disclosed systems and methods can also be practiced in 20 distributed computing environments where tasks or modules are performed by remote processing devices that are linked through a communications network, such as a local area network (LAN), wide area network (WAN), or the Internet, e.g., computing resources provisioned from a “cloud computing” provider. In a distributed computing environment, modules can be located in both local and remote memory storage devices. For example, in some embodiments, the non-contact voltage sensing apparatus **100** includes a sensor configured to capture voltage parameters at a first location, and signal processing circuitry at a second location remote from the first location. Such implementations allow remote voltage sensing around an electrical network at low cost with centralized computational resources.

Alternative implementations of the systems disclosed 25 herein can employ systems having blocks arranged in different ways; and some blocks can be deleted, moved, added, subdivided, combined, and/or modified to provide alternative or sub combinations. Each of these blocks can be implemented in a variety of different ways. However, it is not necessary to show such infrastructure and implementation details or variations in FIG. **1** in order to describe an illustrative embodiment.

FIG. **2** illustrates an exploded isometric view of components of an example non-contact voltage sensing apparatus **200** in accordance with one embodiment. The example non-contact voltage sensing apparatus **200** includes a housing in two parts: an upper housing **210** and a lower housing **215**. The upper housing **210** includes an upper hinge part **214**, and the lower housing **215** includes a lower hinge part **216**. Together, the upper hinge part **214** and the lower hinge part **216** form a hinge that allows the upper housing **210** and the lower housing **215** to hinge open and remain connected, 30



providing an advantageous way to place the non-contact voltage sensing apparatus **200** around a conductor. When the hinges **214**, **216** are engaged and the upper housing **210** and lower housing **215** are closed, a hook **212** on the upper housing **210** engages with a bar **218** on the lower housing **215** to secure the non-contact voltage sensing apparatus **200** around a conductor. The illustrated hinge and closure mechanisms are examples; alternative approaches could include any of a wide variety of mechanisms such as a friction fit or snap fit between the upper housing **210** and lower housing **215**, a screw-on attachment, a magnetic attachment, a locking pin, a fastener securement, a hook-and-loop fabric securement, another style of mechanical latch, etc. Implementations without a split-core current transformer (e.g., with a one-piece transformer core or no current transformer) may have a housing in one part and include no closure mechanism at all.

When the non-contact voltage sensing apparatus **200** is closed, it provides a measurement region **220** for a conductor. In the illustrated embodiment, the measurement region **220** passes through the non-contact voltage sensing apparatus **200**. In other embodiments, the measurement region may be arranged in other ways, such as along a non-contact voltage sensing apparatus, so that the apparatus can measure voltage in a conductor located at or against the apparatus without requiring the conductor to pass through the apparatus.

Adjacent to the measurement region **220** is a conductive sense plate **230**. The conductive sense plate **230** is electrically connected to circuitry or electronics **240** by a connection **235**.

The non-contact voltage sensing apparatus **200** includes a current transformer (e.g., a ferro-magnetic core, such as a ferrite or nanocrystalline core) divided into two parts: an upper core **251** within the upper housing **210**, and a lower core **252** within the lower housing **215**. The upper core **251** and the lower core **252** come together to form a complete loop around the measurement region **220**. In some embodiments, the current transformer (CT) is one piece rather than a split core, which may only partially surround a conductor or may require a conductor to be threaded through the current transformer core. When a conductor is energized in the measurement region **220** and the non-contact voltage sensing apparatus **200** is closed around the conductor, windings **253** around the lower core **252** and connected to the electronics **240** enable the current transformer to sense current through the conductor and/or harvest energy from the conductor.

The present disclosure encompasses various arrangements and shapes of voltage sensing systems, and is not limited to the embodiment described via this illustrative example. FIGS. **11** and **13A-C**, for example, illustrate alternative arrangements.

FIG. **3** illustrates a different exploded breakout view of components of an example non-contact voltage sensing apparatus **300** in accordance with one embodiment. This illustration of an example non-contact voltage sensing apparatus **300** includes elements of the non-contact voltage sensing apparatus **200** of FIG. **2**. For example, it includes the components of the housing: the upper housing **210** and the lower housing **215**, the upper hinge part **214** and the lower hinge part **216**, the hook **212** on the upper housing **210** that engages with the bar **218** on the lower housing **215**. The example non-contact voltage sensing apparatus **300** also includes the measurement region **220**, around which are

situated the upper core **251** and the lower core **252** that form the core of the current transformer (the windings **253** are not shown in this illustration).

In this embodiment, resilient foam pieces **310** are configured to fit within the upper housing **210**, on opposite sides of the current transformer upper core **251**. The resilient foam pieces **310** provide a mechanical spring force to press a conductor in the measurement region **220** toward the conductive sense plate **230** when the non-contact voltage sensing apparatus **300** is assembled and closed around a conductor. In various embodiments, other mechanical means may be employed to fix or locate a conductor within the non-contact voltage sensing apparatus **300**, e.g., a spring or a spring-loaded plate to provide a pushing force on a conductor, or a strap or clip to pull a conductor into a position.

The lower core **252** and an aligner **350** are shown, for illustrative purposes, out of the order in which they would be assembled in this example non-contact voltage sensing apparatus **300**. In operation, the aligner **350** and lower core **252** would be located below the carrier **330** for the conductive sense plate **230**. Similarly, for visibility the electronics **240** are shown broken out outside the lower housing **215**.

In this embodiment, a separator **320** separates the measurement region **220** from the conductive sense plate **230**, and in operation below it the carrier **330**, the aligner **350**, the current transformer lower core **252**, and the electronics **240**. The separator **320** is illustrated as a plastic piece having a thickness of approximately 1 mm. In various embodiments, the separator **320** can be formed of various materials, be of various thicknesses, be of implicit construction (so that a space is provided between the measurement region **220** and the conductive sense plate **230**) or be omitted (so that no space is provided between the measurement region **220** and the conductive sense plate **230**).

In the illustrated embodiment, the conductive sense plate **230** is a conductive metal layer on a flexible printed circuit board ("PCB") with an insulating layer, e.g., polyamide. The connection **235** is made of the same material. The conductive sense plate **230** is shown configured with a curve or the flexibility to curve around a conductor in the measurement region **220** to improve capacitive coupling, e.g., by providing a reduced average distance between the conductive sense plate **230** and the conductor. A conductive sense plate **230** may also be flat (e.g., for simplicity of manufacture) or have a different shape.

In this example embodiment, the electronics **240** include three PCBs **342**, **344**, **346**. In an implementation, each PCB may include circuitry to perform a discrete function or set of functions. For example, the electronics **240** may include a voltage sensing circuitry PCB **342**, an energy harvesting and current sensing circuitry PCB **344**, and a microcontroller and RF communication circuitry PCB **346**. Another embodiment could integrate some or all of these functions onto a single PCB. Yet another embodiment could integrate some or all of these functions into an ASIC.

FIG. **4** illustrates a perspective view of an assembled example non-contact voltage sensing apparatus **400** in accordance with one embodiment. The upper housing **210** and the lower housing **215** of FIG. **2** are closed, and the hook **212** on the upper housing **210** is engaged with the bar **218** on the lower housing **215**. This illustrates an elegant closure by which a person can simply press on the hook **212** to release it from the bar **218** and open the non-contact voltage sensing apparatus **400** (via the hinge, which is not visible) for placing the apparatus **400** onto, or removing it from, a conductor **420**. The example non-contact voltage sensing



## 11

apparatus **400** shows, by dashed line, a conductor **420** located in the measurement region of the apparatus **400**, pressed into a position relative to the conductive sense plate by the mechanical spring force from the resilient foam pieces **310**.

FIG. **5** illustrates an operational routine **500** of a non-contact voltage sensing system in accordance with one embodiment. In various embodiments, the operational routine **500** is performed by one or more non-contact voltage sensing apparatuses such as those illustrated above with reference to FIGS. **1-4**. Portions of the operational routine **500** may be performed by circuitry such as illustrated below with reference to FIGS. **6-9**. As those having ordinary skill in the art will recognize, not all events of an operational routine are illustrated in FIG. **5**. Rather, for clarity, only those aspects reasonably relevant to describing the non-contact sensing of an AC voltage are shown and described. Those having ordinary skill in the art will also recognize that the presented embodiment is merely one example embodiment and that variations on the presented embodiment may be made without departing from the scope of the broader inventive concept set forth in the description herein and the claims below. The operational routine **500** begins in starting block **501**.

In block **515**, the operational routine **500** receives a single AC conductor in or at a measurement region. As described above with reference to FIGS. **1** and **2**, a measurement region for a conductor may be arranged so that the conductor passes along, into, or through the measurement region provided by the housing. The operational routine **500** receives a single AC conductor and excludes other conductors.

In block **525**, the operational routine **500** shields some or all of the measurement region and/or the measurement circuitry or electronics. This allows the operational routine **500** to reduce interference from other conductors that may be nearby, and thus to improve the quality (e.g., precision and accuracy) of voltage measurement relative to a reference potential. For example, in a multiphase (e.g., three-phase) electrical system, conductors of alternate phases may produce unwanted capacitances to a conductive sense plate, as described below with reference to FIG. **12**. In such an environment, arranging shielding to help isolate capacitance to the target conductor can enable the operational routine **500** to provide improved results.

In various embodiments, the electrode or conductive sense plate **130** may be sensitive to shield capacitance or parasitic capacitance between the conductive sense plate **130** and the shield **125**. The operational routine **500** can selectively drive them to the same (or nearly the same) voltage to reduce or eliminate a displacement current between them, as further described below with reference to block **540**.

In block **535**, the operational routine **500** obtains an AC waveform by measuring a current induced via capacitive coupling between the energized conductor in the measurement region and a conductive sense plate of the non-contact voltage sensing apparatus. Example waveform-sensing electronic circuitry is described in further detail with reference to FIG. **7** below. The operational routine **500** may sample an AC waveform, though the sampled waveform may be a filtered and/or distorted representation of a voltage between the energized conductor and a reference potential.

The illustrated operational routine **500** branches to show two alternative approaches to determine a coupling capacitance and/or a scaling factor based on coupling capacitance. One branch includes blocks **540**, **550**, and **560**; the other branch includes blocks **545** and **555**. Various implementa-

## 12

tions of a non-contact voltage sensing system may utilize either approach, or combinations or permutations thereof.

Turning to the approach illustrated in blocks **540**, **550**, and **560**: in some implementations, the routine **500** uses capacitance-determining electronic circuitry to measure a coupling capacitance between the energized conductor in the measurement region and the conductive sense plate of the non-contact voltage sensing apparatus. In block **540**, the routine **500** calibrates the capacitance-determining electronic circuitry. Calibration may be performed under controlled conditions at the time of manufacture. Calibration may also be performed during operation, e.g., to correct for effects of parasitic capacitance. Example calibration circuitry is described in further detail with reference to FIG. **9** below.

In some embodiments, the operational routine **500** minimizes the effects of capacitive coupling or parasitic capacitance between the conductive sense plate **130** and the shield **125**. In some embodiments, the operational routine **500** electrically connects both the conductive sense plate **130** and the shield **125** to the reference potential **145** to allow them to come to the same potential. In some embodiments, the operational routine **500** drives the shield **125** to a voltage of the conductive sense plate **130**, matching or mirroring the voltages to reduce or eliminate an induced displacement current resulting from a voltage difference between them. In some embodiments, the operational routine **500** actively drives a signal into both the conductive sense plate **130** and the shield **125**, driving them with the same voltage potential to eliminate any voltage difference between them, even in the presence of environmental factors that may vary with direction or time.

The driven signal can be produced by a shield driver circuit or chip for capacitance detection. Example capacitance-determining electronic circuitry is described in further detail with reference to FIG. **8** below. In some embodiments, a capacitance measurement chip or circuit is used to drive both the conductive sense plate **130** and the shield **125** with a high frequency (e.g., approximately 25 kHz) signal or waveform that effectively eliminates capacitive coupling between the conductive sense plate **130** and the shield **125** when the operational routine **500** senses the coupling capacitance between the energized conductor and the conductive sense plate **130**. Examples of a capacitance measurement chip or circuit are described in further detail above with reference to FIG. **1**.

In block **550**, the operational routine **500** senses the coupling capacitance between the energized conductor and the conductive sense plate **130**. For example, the routine **500** may determine the coupling capacitance using the capacitance-determining electronic circuitry calibrated in block **540**. In some embodiments, the operational routine **500** produces a value for the coupling capacitance; in other embodiments, the operational routine **500** obtains an indication that does not directly provide a value for the coupling capacitance but may be used to produce a scaling factor for signal processing.

In block **560**, the operational routine **500** determines a scaling factor based at least in part on the coupling capacitance between the conductor and the conductive sense plate of the non-contact voltage sensing apparatus. Example scaling factor- or capacitance-determining electronic circuitry is described in further detail with reference to FIG. **8** below.

Turning to the approach of blocks **545** and **555**: in some implementations, the routine **500** measures a dimension of a conductive wire located in or at the measurement region. In block **545**, the operational routine **500** fixes (or determines)



the location of the conductor received in block **515** and determines a size of the conductor. To facilitate both physical measurement of the conductor and consistent electric measurement of voltage in the conductor, the routine **500** provides a mechanism for holding the conductor in a place or position. Some example mechanisms are described above with reference to FIG. **3** and below with reference to FIG. **11**.

For example, a digital caliper may determine a width or diameter of a conductor including its insulating jacket. In other embodiments, an optical measuring system may determine a size of the conductor. In other embodiments, a measurement device may, e.g., obtain a circumferential measurement of a conductor, or use a shaped aperture (e.g., a vee shape or stepped opening) to locate a conductor according to its size. In some embodiments, the routine **500** determines a wire gauge or cross-sectional area of the conductor based on a measurement of the conductor. For example, the routine **500** may determine that a range of diameters of any conductive wire plus its insulating jacket corresponds to a particular gauge of wire. Thus, even though different brands of conductors may have different thicknesses of insulation and therefore overall diameters, the operational routine **500** can accurately determine a size of the conductive wire to provide an improved contactless determination of a voltage in the conductor.

In block **555**, the operational routine **500** determines a scaling factor or coupling capacitance between the conductor and the conductive sense plate of the non-contact voltage sensing apparatus. In this approach, capacitance-determining electronic circuitry is configured to produce a scaling factor or estimated capacitance from a combination of fixed or known factors (e.g., the size of the conductive sense plate and distance from the conductive sense plate to the measurement region) and measured variables (e.g., the location and/or size of the target hot conductor). The operational routine **500** may determine the scaling factor or coupling capacitance based in part on the determination of the size of the conductor from block **545**, so that the routine **500** accounts for how a gauge of the conductive wire affects the coupling capacitance.

For example, based on the geometry of the measurement space and location of the conductor relative to the conductive sense plate, together with the size of the conductor determined in block **545**, the routine **500** can perform a calculation or use a lookup table to obtain a computed capacitance or scaling factor.

In block **565**, the operational routine **500** performs signal processing with respect to the AC waveform obtained in block **535** and the scaling factor or coupling capacitance determined in block **560** or block **555**. As described above with reference to FIG. **1**, the routine **500** processes the obtained waveform representation and may recover a shape or frequency spectrum of the line voltage waveform. The operational routine **500** processes the coupling capacitance and/or the size of the conductor and may obtain a scaling factor. This may include multiple scaling factors, e.g., scaling factors that are frequency dependent and/or scaling factors that account for different influences on the obtained waveform representation. The operational routine **500** performs signal processing that scales the obtained waveform representation (e.g., the recovered shape or frequency spectrum of the line voltage waveform) based on the coupling capacitance (e.g., according to the scaling factor(s)).

In some implementations, the routine **500** applies one or more scaling factors to account for, e.g., nonlinearities in a circuit, attenuation at particular frequencies, or complex

impedances, to separate out multiple correction factors that may affect measurement. In some implementations, calibration of a circuit may provide an additional scaling factor to account for parasitic capacitance.

In block **575**, the operational routine **500** determines, based on the signal processing in block **565**, an AC voltage of the conductor relative to a reference potential. The operational routine **500** is thus able to determine conductor voltage without interrupting the conductor, without contact to the conductor wire, and without comparison to any other AC signal.

In various embodiments, a non-contact voltage sensing apparatus according to the present disclosure can perform multiple measurements within a single phase, or change phases multiple times in the process of generating a measurement. For example, the operational routine **500** may perform ten to sixty to three hundred individual measurements (each lasting, e.g., one second) to obtain an AC waveform or to determine a coupling capacitance and/or a scaling factor. When determining an AC voltage, the operational routine **500** may use an average to reduce variation; provide a rolling average to smooth time-varying results or sampling errors; or otherwise adjust or process the measurements (e.g., via statistical methods to handle spurious or outlier values) to produce a reliable determination. In some embodiments, the operational routine **500** is configurable among more rapid results, greater sampling volume, and different timing and/or ordering of measurements.

The operational routine **500** ends in ending block **599**.

Alternative implementations of the operational routine **500** can perform routines having processes in a different order, and some processes or blocks can be deleted, moved, added, subdivided, combined, and/or modified to provide alternative or sub combinations. Each of these processes or blocks can be implemented in a variety of different ways. While some processes or blocks may be shown as being performed in series, they may instead be performed or implemented in parallel, or can be performed at different times.

FIG. **6** is a wiring diagram schematically illustrating a multiplexing circuit **600** of electrical components configured to measure a waveform and a capacitance in accordance with one embodiment. A hot conductor **620** carries an AC line current and voltage to be measured by a non-contact voltage sensing apparatus. The line voltage **625** in conductor **620** is labeled " $V_{line}$ " in FIGS. **6-9**. The hot conductor **620** is part of an electrical circuit that typically includes a load (not shown), a neutral **615** (e.g., a line, conductor, bus, or node), and a connection to earth **610**.

The hot conductor **620** is capacitively coupled with a conductive sense plate **630**. The capacitance **635** between the conductive sense plate **630** and the hot conductor **620** is labeled " $C_{sense}$ " in FIGS. **6-9** and **12**. In various embodiments, the conductive sense plate **630** may comprise one or more components of a capacitor such as the conductive sense plate **130** described above with reference to FIG. **1** or the conductive sense plate **230** described above with reference to FIGS. **2-3**.

The conductive sense plate **630** may be switchably connectable to a waveform detector **650** (e.g., waveform-sensing electronic circuitry such as described in further detail with reference to FIG. **7** below) via switch  $S_0$  **640**, and/or to a capacitance detector **660** (e.g., capacitance-determining electronic circuitry such as described in further detail with reference to FIG. **8** below) via switch  $S_1$  **645**. In some embodiments, switches  $S_0$  **640** and  $S_1$  **645** are physically connected or logically controlled so that when switch  $S_0$  **640**



is closed, switch  $S_1$  645 is open, and/or vice versa. For example, switch  $S_0$  640 and switch  $S_1$  645 can be implemented as one single-pole double-throw (“SPDT”) switch. In such embodiments, the conductive sense plate 630 is switched between the waveform detector 650 and the capacitance detector 660 so that the conductive sense plate 630 is connected to either the waveform detector 650 or the capacitance detector 660 but not to both at the same time.

In some embodiments, switches  $S_0$  640 and  $S_1$  645 can be switched independently, e.g., allowing both to be in an open state so that the conductive sense plate 630 is connected to neither the waveform detector 650 nor the capacitance detector 660. In some embodiments, switches  $S_0$  640 and  $S_1$  645 can be switched such that both are in a closed state so that the conductive sense plate 630 is connected to both the waveform detector 650 and the capacitance detector 660 at the same time. In some embodiments, the switches  $S_0$  640 and  $S_1$  645 are connected to separate conductive sense plates 630, such that the waveform detector 650 is switchably connected to one conductive sense plate 630 and the capacitance detector 660 is switchably connected to another conductive sense plate 630.

In an embodiment in which the conductive sense plate 630 is configured to be switchable between the waveform detector 650 and the capacitance detector 660, the switches  $S_0$  640 and  $S_1$  645 may be operated in two or more stages or phases. For example, in one stage or phase “A”, switch  $S_0$  640 may be closed, and switch  $S_1$  645 may be open, so that the waveform detector 650 can amplify and sample a filtered  $V_{line}$  waveform “ $V_{sense}$ ” 655 of voltage in the hot conductor 620. In another stage or phase “B”, switch  $S_0$  640 may be open, and switch  $S_1$  645 may be closed, so that the capacitance detector 660 can measure capacitance  $C_{sense}$  635 between the conductive sense plate 630 and the hot conductor 620 to obtain a scaling factor 665 for scaling the filtered  $V_{line}$  waveform “ $V_{sense}$ ” 655. The multiplexing circuit 600 may switch additional or different components; for example, the shield 125 of FIG. 1 may also be multiplexed with a shield driver circuit associated with the capacitance detector 660. The shield driver circuit can then drive the shield 125 to the same voltage as the electrode or conductive sense plate 630 (which may require additional circuitry to measure a voltage or baseline bias signal of the electrode or conductive sense plate 630), improving measurement of the capacitance  $C_{sense}$  635.

Accordingly, by controlling the switches  $S_0$  640 and/or  $S_1$  645, a multiplexing circuit 600 of a non-contact voltage sensing apparatus according to the present disclosure can selectively couple a conductive sense plate 630 to a waveform detector 650 and/or a capacitance detector 660. By multiplexing the conductive sense plate 630 between the waveform detector 650 and the capacitance detector 660, the same conductive sense plate 630 used by the waveform detector 650 can be shared with the capacitance detector 660 for accurate measurement and signal processing. In addition, the multiplexing allows duplication of components to be minimized.

FIG. 7 is a wiring diagram schematically illustrating electrical components of a waveform detector circuit 700 in accordance with one embodiment. The waveform detector circuit 700 includes the hot conductor 620 with voltage  $V_{line}$  625, earth 610 (reference voltage), conductive sense plate 630 with capacitance  $C_{sense}$  635, and switch  $S_0$  640 in a closed position, as described in further detail above with reference to FIG. 6. The illustrated waveform detector circuit 700 is configured to convert an induced current “ $i_1$ ” 735 into an amplified voltage signal proportional to the hot

conductor 620 voltage  $V_{line}$  625. The time-varying AC voltage 625 of the hot conductor 620 induces, through capacitive coupling, the induced current  $i_1$  735, so that the waveform detector circuit 700 produces a filtered or distorted  $V_{line}$  waveform output “ $V_{sense}$ ” 655.

In the illustrated embodiment, the waveform detector circuit 700 is implemented as a transimpedance amplifier circuit. Those having ordinary skill in the art will recognize that alternative implementations, e.g., other means of current measurement that may include different current-to-voltage circuitry or other current-sensing circuitry, may equivalently be used to sense the induced current  $i_1$  735.

The illustrated waveform detector circuit 700 includes an amplifier 750, e.g., an op-amp. At one input of the amplifier 750, a constant DC reference voltage “ $V_{ref}$ ” 745 may be used to properly bias the waveform detector circuit 700. At another input of the amplifier 750, the induced current  $i_1$  735 is combined with a feedback loop connected to the output  $V_{sense}$  655. The feedback loop resistance “ $R_f$ ” 755 may be chosen to provide a gain for the amplifier 750. The amplifier 750 is also connected to a DC supply voltage  $V_{CC}$  752 and a sensor ground 751.

The illustrated waveform detector circuit 700 produces an output signal  $V_{sense}$  655 that scales linearly with the coupling capacitance  $C_{sense}$  635 and with the voltage  $V_{line}$  625 in the hot conductor 620. For example, the illustrated circuit may determine the output  $V_{sense}$  655 as follows, based on the time-varying voltage  $V_{line}$  625 in the hot conductor 620, the coupling capacitance  $C_{sense}$  635 between the conductive sense plate 630 and the hot conductor 620, the induced current  $i_1$  735, and the feedback loop resistance  $R_f$  755:

$$\begin{aligned} i_1(t) &= C_{sense} \frac{dv_{line}(t)}{dt} \\ v_{sense}(t) &= -i_1(t)R_f \\ v_{sense}(t) &= -R_f C_{sense} \frac{dv_{line}(t)}{dt} \\ v_{line}(t) &= -\frac{1}{R_f C_{sense}} \int v_{sense}(t) dt \end{aligned}$$

Integrating the determined output  $V_{sense}$  655, the waveform detector circuit 700 or signal processing circuitry produces a response proportional to the time-varying AC line voltage  $V_{line}$  625.

Thus, if the coupling capacitance  $C_{sense}$  635 can be known, the output  $V_{sense}$  655 of the waveform detector circuit 700 can be used by a non-contact voltage sensing apparatus according to the present disclosure to measure the AC line voltage  $V_{line}$  625 in the hot conductor 620.

FIG. 8 is a wiring diagram schematically illustrating electrical components of a capacitance detector circuit 800 (or capacitance-determining electronic circuitry) in accordance with one embodiment. The capacitance detector circuit 800 includes the hot conductor 620 with voltage  $V_{line}$  625, earth 610 (reference voltage), and conductive sense plate 630 with capacitance  $C_{sense}$  635, as described in further detail above with reference to FIG. 6. The illustrated capacitance detector circuit 800 includes node A 825 and node B 830 to illustrate the formation of capacitance  $C_{sense}$  635 in the conductive sense plate 630. In the illustrated embodiment, the metallic wire of the energized hot conductor 820 forms node A, and a conductive sense plate (e.g., the conductive sense plate 130 described above with reference to FIG. 1 or the conductive sense plate 230 described above with reference to FIGS. 2-3) forms node B. The capacitance

$C_{sense}$  635 is dependent on physical characteristics of node A 825 and node B 830, such as, e.g., a size (e.g., wire gauge) of the node A 825 hot conductor 820 and an area and/or shape of the node B 830 conductive sense plate. The capacitance  $C_{sense}$  635 is also dependent on a geometry of a relationship between node A 825 and node B 830, such as, e.g., alignment and distance between node A 825 and node B 830. Such factors may differ with each installation or application of a non-contact voltage sensing apparatus according to the present disclosure. Therefore, a capacitance detector circuit 800 allows more accurate determination of the voltage  $V_{line}$  625 in the hot conductor 620.

The illustrated capacitance detector circuit 800 includes a relaxation oscillator configured to generate a signal having a frequency proportional to the capacitance  $C_{sense}$  635 between the hot conductor 620 and the conductive sense plate 630. The conductive sense plate 630 is discharged by current flow in the following loop: node B 830, sensor ground 851, earth 610, neutral, node A 825. The conductive sense plate 630 is charged by current flow in the following loop: node B 830,  $V_{CC}$  852, sensor ground 851, earth 610, neutral, node A 825. The capacitance detector circuit 800 produces a voltage output “ $V_{out}$ ” 860 that switches at a switching frequency  $fv_{out}$  865. The switching frequency  $fv_{out}$  865 of the capacitance detector circuit 800 output  $V_{out}$  860 can provide a scaling factor 665 for scaling the filtered  $V_{line}$  waveform output  $V_{sense}$  655 from the waveform detector circuit 700.

In the illustrated embodiment, the capacitance detector circuit 800 is implemented as an astable multivibrator circuit. Those having ordinary skill in the art will recognize that alternative implementations, e.g., other means of capacitance measurement that may include different relaxation oscillator or capacitance-to-frequency circuitry or other capacitance-sensing circuitry, may equivalently be used to sense the capacitance  $C_{sense}$  635. The illustrated relaxation oscillator circuit allows a non-contact voltage sensing apparatus in accordance with this disclosure to synthesize a transfer function to easily recover the  $V_{line}$  waveform from the filtered  $V_{sense}$  655, at a low power expenditure.

The illustrated capacitance detector circuit 800 is astable and continuously switches its output  $V_{out}$  860 between  $V_{CC}$  852 and the sensor ground 851 potential (e.g., connected to earth 610 or another reference potential). The astable multivibrator circuit includes an op-amp 850, a feedback resistance  $R_f$  840, a constant DC reference voltage  $V_{ref}$  842, and resistances  $R_1$  841 and  $R_2$  842. Its output  $V_{out}$  860 switching frequency  $fv_{out}$  865 depends on a time constant set by feedback resistance  $R_f$  840 and the coupling capacitance  $C_{sense}$  635 formed between the hot conductor 620 and the conductive sense plate 630. For example, the switching frequency  $fv_{out}$  865 of the illustrated circuit 800 is inversely proportional to  $C_{sense}$  635. Accordingly, the capacitance detector circuit 800 may determine the switching frequency  $fv_{out}$  865 as follows:

$$\beta = \frac{R_2}{R_1 + R_2}$$

$$T_{V_{out}} = 2R_f C_{sense} \ln\left(\frac{1 + \beta}{1 - \beta}\right)$$

$$f_{V_{out}} = \frac{1}{T_{V_{out}}}$$

Signal processing electronic circuitry may be configured to use the output frequency  $fv_{out}$  865 of the coupling

capacitance-determining electronic circuitry 800 to obtain a determination of the capacitance  $C_{sense}$  635 and apply that determination to scale the filtered  $V_{line}$  waveform output  $V_{sense}$  655 produced by the waveform detector circuit 700, which depends on the capacitance  $C_{sense}$  635.

In some embodiments, a capacitance detector circuit 800 includes a shield driver circuit or chip and/or a capacitance measurement chip or circuit such as those described above with reference to FIG. 1.

FIG. 9 is a wiring diagram schematically illustrating electrical components of a calibration circuit 900 configured to calibrate a capacitance detector circuit in accordance with one embodiment. In the illustrated embodiment, the calibration circuit 900 includes a capacitance detector 950 that can be calibrated to more accurately measure a capacitance, e.g., the capacitance  $C_{sense}$  635. For example, the capacitance detector 950 may include a portion or all of the capacitance detector circuit 800 described above with reference to FIG. 8 (e.g., a relaxation oscillator).

It also includes two capacitive elements: a fixed, known, or background (e.g., parasitic [possibly unknown and/or changing]) capacitance  $C_{par}$  935 between a ground or reference potential and the capacitance detector 950, and the possibly variable or unknown coupling capacitance  $C_{sense}$  635 formed between the hot conductor 620 and the conductive sense plate 630. The calibration circuit 900 also includes a calibration stage or phase switch “ $S_1$ ” 940. The illustrated calibration circuit 900 is configured to operate in two stages or phases (not to be confused with the phases of multiphase AC power) to calibrate the capacitance detector 950.

In Stage or Phase A, the calibration stage or phase switch  $S_1$  940 is open, and the capacitance detector 950 is only influenced by the capacitance  $C_{par}$  935. In Stage or Phase A, the capacitance detector 950 is isolated from the coupling capacitance  $C_{sense}$  635. Accordingly, the output (e.g., frequency) of the capacitance detector 950 in Stage or Phase A is proportional to the capacitance  $C_{par}$  935.

In Stage or Phase B, the calibration stage or phase switch “ $S_1$ ” 940 is closed, so that the coupling capacitance  $C_{sense}$  635 is also connected into the circuit including the capacitance  $C_{par}$  935 and the capacitance detector 950. Accordingly, the output (e.g., frequency) of the capacitance detector 950 in Stage or Phase B is proportional to both the capacitance  $C_{par}$  935 and the coupling capacitance  $C_{sense}$  635. In the illustrated embodiment, the frequency of the capacitance detector 950 in Stage or Phase B is proportional to the sum of capacitance  $C_{par}$  935 and coupling capacitance  $C_{sense}$  635.

By comparing or otherwise combining or applying the output of the capacitance detector 950 in Stage or Phase A with the output of the capacitance detector 950 in Stage or Phase B, the calibration circuit 900 (or, e.g., signal processing circuitry and/or control circuitry) can obtain a more accurate determination of the coupling capacitance  $C_{sense}$  635. For example, in the illustrated embodiment, calibration may include taking a difference between two frequencies:  $C_{sense} \propto (f_B - f_A)$ .

The calibration circuit 900 provides a way to dynamically correct for the effect of any parasitic capacitance  $C_{par}$  935, and/or to calibrate a capacitance detector 950. In other implementations, such a correction may be performed by a different type of calibration circuit, e.g., calibration via controlled conditions at manufacturing.

FIGS. 10A-10B are graphs illustrating a sensitivity of sensed capacitance to conductor size and distance from a conductive sense plate, for a given dielectric constant.

FIG. 10A illustrates a graph 1000 showing a modeled relationship between distance and capacitance  $C_{sense}$  for



wires of different gauges. The x-axis of graph 1000 displays a distance “d\_wire\_plate” 1020 between a conductive sense plate and a conductive wire, measured in millimeters (ranging linearly from approximately 1 mm to 20 mm in divisions of 2.5 mm). The y-axis of graph 1000 displays a capacitance “C\_sense” 1030, measured in Farads (ranging from approximately  $10^{-14}$  to  $10^{-11}$  Farads, in a logarithmic or other non-linear scale). Capacitance-versus-distance curves are plotted for four wires of different sizes: 6-gauge (AWG6) wire 1006, 8-gauge (AWG8) wire 1008, 10-gauge (AWG10) wire 1010, and 12-gauge (AWG12) wire 1012. For a given wire, capacitance is greater for a smaller distance. For a given distance between the sense plate and wire, capacitance is greater for larger wire.

FIG. 10B illustrates a graph 1050 showing a modeled relationship between wire positioning error and percent absolute error of measuring voltage  $V_{sense}$  in wires of different gauges. The x-axis of graph 1050 displays a distance “d\_wire\_plate” 1070 between a conductive sense plate and a conductive wire, measured in millimeters (ranging linearly from approximately 9 mm to 11 mm in divisions of 0.25 mm). The y-axis of graph 1050 displays a “Percent Error Amplitude( $V_{sense}$ )” 1080, measured in percentages (ranging linearly from 0 to 20 percent). Error-versus-distance curves are plotted for four wires of different sizes: 6-gauge (AWG6) wire 1056, 8-gauge (AWG8) wire 1058, 10-gauge (AWG10) wire 1060, and 12-gauge (AWG12) wire 1062. The curves are all calibrated for a target 10-millimeter distance from the conductive sense plate to the center of the wire, so all of the curves show no error where d\_wire\_plate is exactly 10 mm. For a given wire, as actual distance to the sense plate diverges in either direction from the calibrated distance, the absolute value of the error percentage grows larger. For a given distance between the sense plate and wire, percentage error is greater for larger wire.

FIG. 11 illustrates physical components of an example conductor fixing and measurement system 1100 including a digital caliper in accordance with one embodiment. A conductor fixing and measurement system 1100 may improve measurement of a capacitance  $C_{sense}$  and reduce error in determining an AC voltage  $V_{sense}$  (e.g., as illustrated above with reference to FIGS. 10A-10B), for example by enabling a non-contact voltage sensing apparatus to determine and/or account for a location of the conductor to be measured and a size of the conductor to be measured.

In some embodiments, the non-contact voltage sensing apparatus of the present disclosure includes conductor measurement means to fix and/or measure one or more aspects of a conductor at a measurement region. For example, the apparatus may include one or more features configured to guide a conductor to the measurement region (e.g., to a location and/or into an orientation at the measurement region) and/or to hold the conductor at or in the measurement region. In some embodiments, the apparatus is configured to fix at least a portion of a conductor in or against a known position.

The apparatus may include one or more features to obtain a determination of at least one physical dimension of the conductor. For example, the apparatus may be configured to determine a diameter of a conductor (e.g., a wire including an outer insulating jacket/layer), a circumference of the conductor (e.g., a partial circumference), a circumferential curvature of the conductor, a wire gauge of the conductor, and/or a cross-sectional area of the conductor.

In the illustrated example, a conductor fixing and measurement system 1100 includes a digital caliper. The system

1100 includes an upper housing 1110 and a lower housing 1115 connected by a hinge 1116. The upper housing 1110 and lower housing 1115 close around a measurement region 1120 configured to receive a conductor 1122. The conductor 1122 is pressed between a fixed caliper jaw 1130 within the lower housing 1115 and a movable caliper jaw 1140 (e.g., slidable) within the upper housing 1110. The movable caliper jaw 1140 is connected to a pair of guide rails 1145 that can move within rail receivers 1140 in the upper housing 1110, allowing the movable caliper jaw 1140 to adjust to accommodate different sizes of conductor 1122. A tension leaf spring 1160 or other resilient element provides spring force to move or press the movable caliper jaw 1140 against the conductor 1122.

In operation, the conductor fixing and measurement system 1100 includes a sliding measure 1170 (e.g., attached to or part of a guide rail 1145) that indicates, by the location of the movable caliper jaw 1140, the size (e.g., diameter) of the conductor 1122. For example, the sliding measure 1170 may include conductive, capacitive, resistive, magnetic, and/or optical elements readable by an electrical contact, magnetic head, or optical reader 1180. For example, the sliding measure 1170 may include a PCB with metallic fingers at a periodic spacing, and the reader 1180 may include a conductive sense electrode and/or capacitance detector circuit (e.g., on another PCB). When the measure 1170 PCB moves with respect to the reader 1180, the capacitance changes periodically as the conductive fingers (e.g., triangles) of the sliding measure 1170 slide past the reader 1180. A microcontroller can count the periodic changes in capacitance corresponding to the changing positioning of the sliding measure 1170 attached to the movable caliper jaw 1140. Thus, based on the known finger spacing and the count of capacitance changes, the microcontroller may determine an absolute positioning of the movable caliper jaw 1140 with respect to the reader 1180. This allows precise measurement of the diameter of the conductor 1122. In some embodiments, the conductor fixing and measurement system 1100 includes an absolute positioning identification system (e.g., a binary code reader) that incorporates mechanical, electromagnetic, and/or optical position coding.

From the total diameter of the conductor 1122 (including approximately twice the thickness of its insulating jacket), the microcontroller can calculate a probable wire gauge and probable insulation thickness. For example, known insulation and/or wire gauge standards may enable the conductor fixing and measurement system 1100 to categorize the conductor into one of a set of discrete categories, e.g., if a thickest 6-gauge wire is smaller than a thinnest 4-gauge wire. Based on those calculations, the conductor fixing and measurement system 1100 can estimate a distance between the center of the wire and the conductive sense plate.

A non-contact voltage sensing apparatus may include a conductor fixing and measurement system 1100 or a functional equivalent to improve the accuracy of determining a coupling capacitance between a target conductor and a conductive sense plate, so that the apparatus provides a more accurate determination of an AC voltage in the target conductor.

FIG. 12 is a wiring diagram 1200 schematically illustrating multiphase coupling capacitances. Conventionally, shielding (such as shield 125 described above with reference to FIG. 1) has not been considered necessary in measuring an AC circuit. The inventors have discovered, however, that shielding can be surprisingly important for non-contact voltage sensing in multiphase (e.g., three-phase) environments.



For example, without shielding, a current can undesirably be injected into a waveform detector **650** from an energized non-target AC voltage phase. The wiring diagram **1200** schematically illustrates an example multiphase environment in which the waveform detector **650** is intended to measure the voltage on a first conductor  $V_A$  **1220** with respect to a ground **1210** potential. The multiphase environment includes additional conductors  $V_B$  **1230** and  $V_C$  **1240** energized with AC voltages of different phases. As a result, the waveform measured by waveform detector **650** may be corrupted by capacitances **1235**, **1245** between the waveform detector **650** and conductors  $V_B$  **1230** and  $V_C$  **1240**, and potentially capacitances **1237**, **1247** between the sensor ground **1215** potential and conductors  $V_B$  **1230** and  $V_C$  **1240**. As a result of the currents injected from these non-target phases, the output  $V_{sense}$  **655** may be incorrect. Therefore, the disclosed non-contact voltage sensing apparatus is shielded to reduce the influence of undesired capacitances as described above.

In addition, as described above, the undesirable effects of capacitance between the shielding itself and the electrode (such as the conductive sense plate **130** described above with reference to FIG. 1) can be negated by actively driving the shielding to the same potential as the electrode.

FIGS. **13A-13D** illustrate schematic, perspective, and sectional views of example non-contact voltage sensing apparatuses having a flexible sensing attachment in accordance with various embodiments.

FIG. **13A** illustrates a schematic top or bottom view of an example non-contact voltage sensing apparatus **1300A** having a flexible sensing attachment arranged in an extended state. Various components may be mounted on the top and/or bottom of the apparatus **1300A** as appropriate to the implementation and application. The apparatus **1300A** includes an electrode or conductive sense plate **1330**. The electrode or conductive sense plate **1330** is configured to form a capacitive coupling with a conductor when deployed in an alternative state such as depicted in FIG. **13B** or FIG. **13C**. The electrode or conductive sense plate **1330** is electrically connected to circuitry or electronics **1340** by a bus or connection **1335**. In various embodiments, the bus or connection **1335** may be a wire, a trace on a PCB (e.g., a flexible PCB), etc. The electrode or conductive sense plate **1330** and the bus or connection **1335** are mounted on a flexible substrate **1325** portion of the flexible sensing attachment. The flexible substrate **1325** portion of the flexible sensing attachment is constructed of metal (e.g., a thin strip of flexible spring steel), plastic, fabric, tape, or another suitable material. In various embodiments, the flexible substrate **1325** portion of the flexible sensing attachment is electrically conductive or includes a shielding layer. In such embodiments, the electrode or conductive sense plate **1330** and the bus or connection **1335** are insulated from the flexible substrate **1325**. This can be accomplished in various ways, such as by putting the electrode or conductive sense plate **1330** and the bus or connection **1335** on a flex-PCB in which the PCB dielectric serves as the insulator; or by insulating the flexible substrate **1325** with a material such as paint, plastic, fabric, or silicone rubber (in some embodiments, the electrode or conductive sense plate **1330** and the bus or connection **1335** could then be directly applied to the insulative material). A schematic example of shielding an electrode is described below with reference to FIG. **13D**, which corresponds to a section of the flexible substrate **1325** of the non-contact voltage sensing apparatus **1300A** along line **13D-13D**.

In the illustrated embodiment, the electrode or conductive sense plate **1330** is a conductive metal layer on a flexible PCB with an insulating layer, e.g., polyamide, and the bus or connection **1335** is an extension of the conductive metal layer or a flex cable that can be made of the same or a different material. The electrode or conductive sense plate **1330** is configured with flexibility to curve with the flexible substrate **1325** portion of the flexible sensing attachment. In particular, the electrode or conductive sense plate **1330** is constructed to withstand being in both the extended state of the apparatus illustrated in FIG. **13A** and a curled or wrapped state such as depicted in FIG. **13B** or FIG. **13C**. In various embodiments, the electrode or conductive sense plate **1330** is flexible in multiple directions. For example, it can be flat or curved (concave or convex) along a longitudinal axis of the flexible substrate **1325** portion of the flexible sensing attachment (e.g., when the apparatus **1300A** is in an extended state). In contrast, it can be curled around a transverse axis such as the axis of a conductor perpendicular to the longitudinal axis (e.g., when the apparatus **1300A** is in a curled or wrapped state, such as encircling such a conductor).

In this example embodiment, the electrode or conductive sense plate **1330** is connected via the connection **1335** to components such as electronics **1340**, radio frequency communication circuitry **1375** (which may include an antenna), and a connection interface **1377** (e.g., a wired communication port, a power connection to a battery, a split-core current harvester, a power harvesting circuit, etc.). In some embodiments, the connection interface **1377** includes a link to an antenna or radio transmitter that can be located remotely from the apparatus **1300A**, such as outside an electrical panel within which the apparatus **1300A** is attached to a conductor. The electronics **1340** and the radio **1375** may include or be implemented as one or multiple PCBs, microchips, ASICs, etc. The components may be in communication with other non-contact voltage sensing apparatuses; with a remote base station, measurement device, or data collection or storage system; or with one or more computing devices via one or more communication networks.

In some embodiments, the electronics **1340**, radio frequency communication circuitry **1375**, and connection interface **1377** components of the apparatus **1300A** are implemented in or are mounted on a flexible PCB, or are otherwise flexibly connected to the flexible substrate **1325** portion of the flexible sensing attachment. Mounting them to a flex-PCB, for example, allows them to be produced together with the electrode or conductive sense plate **1330** and the connection **1335**, and for those components to be shielded in common. In some embodiments, those components are mounted to a rigid substrate **1328**. A single substrate may be flexible (e.g., flexible substrate **1325**) on one side of a dividing region **1327** and stiffened or otherwise effectively non-flexible (e.g., rigid substrate **1328**) on an opposite side of the dividing region **1327**. The rigid substrate **1328** may be non-flexible in only one direction or in multiple directions. The dividing region **1327** may include a mechanism such as a rigid piece that holds the otherwise flexible substrate **1325** in a way that prevents the flexible substrate **1325** from bending or flexing, or prevents a bending stimulus from being transmitted past the dividing region **1327** to the effectively rigid substrate **1328**. In some embodiments, the rigid substrate **1328** is surrounded by a housing **1310**. The housing **1310** can function as the mechanism of the dividing region **1327** that keeps the rigid substrate **1328** from being flexed.



FIG. 13B illustrates a perspective view of an example non-contact voltage sensing apparatus 1300B having a flexible sensing attachment arranged in a partly extended and partly curled or wrapped state. The illustrated embodiment includes a bi-stable structure. A bi-stable structure such as a bi-stable spring has two distinct stable equilibrium configurations, and can be transformed from one configuration to the other by passing through an unstable intermediate state. Thus, a device such as apparatus 1300B including a bi-stable structure can be set in either configuration. In the illustrated embodiments of FIGS. 13A-13D, apparatus 1300A of FIG. 13A is in an extended state, and apparatus 1300C of FIG. 13C is in a curled state.

Examples of bi-stable structures may be found in non-analogous contexts such as Venus flytrap plants and slap bracelet or “slap wrap” fashion accessories. A slap bracelet can be constructed of a flexible metal or plastic band (or layered bands), which may be encased or covered by a fabric or rubber (e.g., silicone, urethane, or another elastic material) outer cover. A typical slap bracelet is long enough to wrap completely, but loosely, around a teenager’s wrist (e.g., about nine inches) and wide enough to comfortably display as a wrist decoration (e.g., about an inch or two). The apparatus 1300B, by contrast, is configured to wrap around an electrical conductor, rather than a person’s wrist; and to curl tightly enough to keep the electrode or conductive sense plate 1330 located close to (in some embodiments, at a consistently reproducible or measurable functional distance from or against) the conductor rather than to provide a loosely comfortable bracelet. The apparatus 1300B can be configured to have sufficient width to shield the electrode or conductive sense plate 1330 from interference from other conductors or the environment, which is not a consideration in slap bracelets.

The apparatus 1300B includes a construction incorporating a bi-stable structure. A flexible substrate 1325 in its extended state is curved around a longitudinal axis 1326 that gives the flexible substrate 1325 a trough shape. The flexible substrate 1325 in its curled or wrapped state is curved around an orthogonal transverse axis 1321 that gives the flexible substrate 1325 a loop or cylindrical shape. The transverse axis 1321 generally coincides with a measurement region 1320 that is configured to receive a conductor such as a single insulated copper wire carrying an AC voltage. In the embodiments of FIG. 13, the flexible substrate 1325 forming the flexible sensing attachment is external to any housing 1310. The flexible sensing attachment, rather than the housing 1310, thus provides the measurement region 1320. In various embodiments, the measurement region 1320 is defined by the wrap or curl of the flexible sensing attachment around the conductor, such that there is little or no extra space between the conductor and the electrode or conductive sense plate 1330 where the conductor passes along, into, or through the measurement region 1320. Because the geometry of the electrode or conductive sense plate 1330 on the flexible substrate 1325 changes from longitudinally convex in the extended state to transversely concave in the curled or wrapped state, the electrode or conductive sense plate 1330 must be flexible and resistant to fatigue.

In the illustrated embodiments of FIGS. 13A-13D, the non-contact voltage sensing apparatuses 1300A, 1300B, and 1300C include a shield (see shield 125, described above with reference to FIG. 1) integrated into the flexible substrate 1325. The flexible substrate 1325 may be constructed of material having high conductivity, such as a metallic foil or mesh. In various embodiments, the shield of the flexible

substrate 1325 forms a Faraday cage around a portion of the conductor and the electrode or conductive sense plate 1330 where the conductor passes along, into, or through the measurement region 1320. The shielding can take the form of a wrap, cover, blanket, cylinder, partial tube, etc. rather than a fully enclosing cage. In some embodiments, the shield of the flexible substrate 1325 (which may include the flexible substrate 1325 itself) is connected to a ground potential or actively driven as described above with reference to FIG. 5 to reduce environmental effects on voltage or capacitance measurements.

Transformation of a bi-stable structure from one configuration to the other may be achieved by various stimuli such as mechanical actuation, electrical stimulation, or heating/cooling. Different stimuli (or different applications of one kind of stimulus) may be required or used for the opposite transformation through the intermediate state between two configurations, such as by elastic deformation. Where the bi-stable structure is a spring or is spring-loaded, the transformation can be sudden once the stimulus sends the bi-stable structure past a certain intermediate point. The speed and/or energy of the transformation, and the stiffness or resistance to changing configurations, can be configured in the manufacture or arrangement of the bi-stable structure. The apparatus 1300B is manufactured so that, when the apparatus 1300B is in an extended state, beginning to bend it across or around a conductor causes the apparatus 1300B to bend past a point where it changes state to curl or wrap around the conductor. For example, bending the flexible substrate 1325 so that its curvature around the longitudinal axis 1326 is largely eliminated, leaving it roughly flat between the longitudinal edges, allows the flexible substrate 1325 to wrap around the transverse axis 1321 and the target conductor. The flexible substrate 1325 will stay in that curled state until uncurled. Once fully uncurled into its other bi-stable configuration, the flexible substrate 1325 remains in its extended state until again bent.

For example, to apply the apparatus 1300B to a conductor (e.g., an overhead conductor), a tool such as a “hot stick” (a long, insulated pole that can grab or attach to a housing of the apparatus 1300B) can press or strike the flexible substrate 1325 in an extended state against the conductor, causing the flexible substrate 1325 to wrap around the conductor and become set in a configuration for voltage measurement. To remove the apparatus 1300B from the conductor, the apparatus 1300B can be pulled along the longitudinal axis 1326 to straighten the flexible substrate 1325 and disconnect it from the conductor. In some embodiments, a lever, cable or string, or other mechanism or impetus can straighten the flexible substrate 1325. This allows for a convenient method of attaching a non-contact voltage sensing apparatus to a conductor in a way that was previously unavailable.

Although the embodiments of FIGS. 13B and 13C are described as including a bi-stable structure, the apparatuses of FIGS. 13A-13D could include or be mounted on any flexible substrate. For example, a soft substrate such as a plastic- or tape- or fabric-based attachment could be manually applied to a conductor and secured with any suitable attachment, such as a snap, a clip, a tape such as electrical tape, a peelable adhesive, or a hook-and-loop securement similar to a blood pressure cuff. As another example, a flexible substrate 1325 could include a semi-rigid hook and a vice-like securing device on a slider.

The rigid substrate 1328 of non-contact voltage sensing apparatus 1300B is a rigid PCB attached to the flexible substrate 1325. The inclusion of a rigid PCB allows use of



lower-cost commodity components and connections (e.g., electronics 1340, radio frequency communication circuitry 1375, and connection interface 1377 because they will not be subjected to bending stresses or fatigue, do not require mounting on a flexible PCB, and do not require consideration of bending in board design or component placement. Various approaches to mounting and/or connecting the rigid substrate 1328 and its components to the flexible substrate 1325 are contemplated, including assorted versions of tab-and-slot attachments, friction fitting, adhesive mounting, one or more mechanical fasteners, and mounting of a housing 1310 (e.g., a plastic snap-on cover or hinged box, not shown in FIG. 13B) around or to the rigid substrate 1328 and/or the flexible substrate 1325. In the illustrated example, the rigid substrate 1328 is shown for ease of illustration on the opposite side of the apparatus 1300B from the electrode or conductive sense plate 1330; in various embodiments, elements may be arranged in different ways relative to one another.

In various embodiments, the non-contact voltage sensing apparatus 1300B is configured so that the electrode or conductive sense plate 1330 has a determined or otherwise determinable geometric relationship to the conductor—e.g., so that the electrode (which may include a pad or spacer of known thickness) is pressed against the exterior of the insulating cover of the conductor—when the measurement region 1320 receives the conductor or when the flexible substrate 1325 is wrapped around the conductor. In some embodiments, the non-contact voltage sensing apparatus 1300B is configured to automatically position the electrode or conductive sense plate 1330 with respect to the conductor, such as by causing the flexible substrate 1325 to wrap the conductor (and, e.g., slide against itself as necessary) without leaving a gap therebetween. In such embodiments, the non-contact voltage sensing apparatus 1300B improves capacitive coupling by providing a consistent and minimal average distance between the curled conductive sense plate 1330 and the target conductor.

In various embodiments, the non-contact voltage sensing apparatus 1300B is configured to provide accurate measurement without requiring the electrode or conductive sense plate 1330 to be precisely positioned, or to have a measured or measurable geometry between it and the conductor. As described in further detail above with reference to FIGS. 5, 8, and 9, measurement of the coupling capacitance (using one of multiple approaches) may be accomplished whether or not such a determined or determinable geometric relationship exists. For example, if the electrode or conductive sense plate 1330 is close to the conductor being measured and the flexible substrate 1325 includes a properly situated shield plane (e.g., on the opposite side of the electrode or conductive sense plate 1330 from the conductor), the non-contact voltage sensing apparatus 1300B largely shields the electrode or conductive sense plate 1330 from nearly all external electric fields.

FIG. 13C illustrates a perspective view of a flexible sensing attachment of a non-contact voltage sensing apparatus 1300C arranged in a curled or wrapped state. In the illustrated embodiment, the measurement region 1320 is configured to contain a conductor, with the curled flexible substrate 1325 wrapped around the conductor and the electrode or conductive sense plate 1330 situated on or near the conductor. In various embodiments or applications, the electrode or conductive sense plate 1330 on the inside of the curled flexible substrate 1325 may only wrap around part of the conductor, or only enough to place the electrode or conductive sense plate 1330 against the conductor or oth-

erwise into an expected geometric relationship with the conductor. In the illustrated embodiment, the curled flexible substrate 1325 forms or includes an electromagnetic shield outside the electrode or conductive sense plate 1330 and the conductor in the measurement region 1320, shielding the measurements performed by the apparatus 1300C as described above. The electrode or conductive sense plate 1330 may be placed at or close to the end of the flexible substrate 1325; such placement requires less wrapping of the flexible substrate 1325 to establish reliable positioning of the apparatus 1300C for measurement of the conductor. The electrode or conductive sense plate 1330 may be placed at a distance offset from the end of the flexible substrate 1325, as illustrated in FIGS. 13A and 13C; such placement may reduce bending stress and potential wear and improve long-term reliability of the apparatus 1300C.

Conductors come in different sizes. In some embodiments, the flexible substrate 1325 or another portion of the non-contact voltage sensing apparatus 1300C is configured to measure a size of the conductor and/or an amount of wrapping or curling of the flexible substrate 1325. For example, the flexible substrate 1325 can include a circumference detection sensor 1380 to detect a circumference marker 1385 so that the circumference of the flexible substrate 1325 wrapped around the conductor can be known. As with the sliding measure 1170 described above with reference to FIG. 11, implementations of such a sensor 1380 may include conductive, capacitive, resistive, magnetic, and/or optical elements readable by an electrical contact, magnetic head, or optical reader. For example, one implementation could be similar to a digital dial caliper. Another could operate as a variable resistor or potentiometer, employing a resistive surface or trace on the flexible substrate 1325 and an electrical contact as the sensor 1380 that would be the wiper, so that a distance from one end or the other of the resistive surface or trace to the sensor 1380 could be measured electrically in either ratiometric or absolute terms. From that, the circumference and the diameter and the probable gauge of the conductor can be determined. As another example, the flexible substrate 1325 can include a bending sensor or bending strain gauge to determine how tightly the flexible substrate 1325 is curled to measure a conductor in the measurement region 1320 (or to determine that the measurement region 1320 does not contain a conductor, or does not contain a conductor of sufficient size to produce a close fit for accurate measurements). In some embodiments, the flexible substrate 1325 includes a strain gauge or other sensor to determine whether the apparatus 1300C is in an extended state or a curled or wrapped state, and to activate the apparatus 1300C only if it is in a configuration arranged to be in contact with a conductor.

In some embodiments, some or all of the electronics 1340 (shown and described in further detail above with reference to FIGS. 13A and 13B) are located on the flexible substrate 1325 such that they are wrapped up in the layers or loops of the flexible substrate 1325 when it is curled as depicted in FIG. 13C. This construction can result in the electronics 1340 being sandwiched by one or more layers of shield on all sides. After the electronics 1340 have processed signals (e.g., AC waveform acquisition and/or capacitance measurements), the output can be either digital or low-impedance analog, and thus suitable for routing outside the shielding with much reduced sensitivity to undesired capacitive coupling or interference.

FIG. 13D is a schematic sectional diagram 1300D illustrating a section of the flexible substrate 1325 of the non-contact voltage sensing apparatus 1300A of FIG. 13A along



line 13D-13D. The sectional diagram 1300D shows an example structure of layers shielding the electrode or conductive sense plate 1330. The layers include a metallic or otherwise electrically conductive shielding layer 1350 and an insulative layer 1360. In some embodiments, the shielding layer 1350 includes or is formed of or by multiple metallic layers, such as shown in FIG. 13D. In some implementations, the shielding layer 1350 wraps around the insulative layer 1360 or includes a connection between multiple metallic layers and is not interrupted at the edge of the flexible substrate 1325. The insulative layer 1360 prevents the shielding layer 1350 from contacting the electrode or conductive sense plate 1330. The electrode or conductive sense plate 1330 is quasi-surrounded with the shield on all sides except downward (in the illustrated example), in the direction of the target conductor. In various implementations, the same shielding structure can shield the bus or connection 1335.

Although specific embodiments have been illustrated and described herein, it will be appreciated by those of ordinary skill in the art that alternate and/or equivalent implementations may be substituted for the specific embodiments shown and described without departing from the scope of the present disclosure. For example, although various embodiments are described above in terms of a housing that snaps around a conductor or a flexible sensing attachment that wraps around a conductor, in other embodiments various other form factors may be used. In addition, processing and/or output readings may be provided locally at the apparatus and/or performed or displayed remotely. The spirit and scope of this application is intended to cover any adaptations or variations of the embodiments discussed herein.

Thus, although the subject matter has been described in language specific to structural features and/or methodological acts, it is also to be understood that the subject matter defined in the appended claims is not necessarily limited to the specific features or acts described. Rather, the specific features and acts are disclosed as example forms of implementing the claims. This application is intended to cover any adaptations or variations of the embodiments discussed herein.

#### EXAMPLES

Example 1: A non-contact electric potential meter system suitable for obtaining a determination of a voltage between a first hot conductor of a first alternating current (AC) electrical circuit and a reference potential, without direct electrical contact to the first hot conductor and without comparison to a second AC voltage signal, the non-contact electric potential meter system comprising:

a measurement region configured to receive the first hot conductor without interruption of the first hot conductor; and

a capacitive AC voltage sensing mechanism, comprising:

an electrode situated near the first hot conductor when the measurement region has received the first hot conductor;

an electrical connection connectable to a reference potential;

waveform-sensing electronic circuitry configured to obtain an AC voltage waveform induced by capacitive coupling between the first hot conductor and the electrode; and

capacitance-determining electronic circuitry configured to obtain a scaling factor based on a coupling capacitance formed between the first hot conductor and the electrode; and

signal processing electronic circuitry configured to obtain, from the AC voltage waveform obtained by the waveform-sensing electronic circuitry and the coupling capacitance-based scaling factor obtained by the capacitance-determining electronic circuitry, the voltage between the first hot conductor and the reference potential.

Example 2: The non-contact electric potential meter system of Example 1, wherein the measurement region is configured such that no other conductor is received by the measurement region.

Example 3: The non-contact electric potential meter system of any of Examples 1-2, wherein the electrode is mounted to, connected to, or formed in or by a flexible PCB.

Example 4: The non-contact electric potential meter system of any of Examples 1-3, wherein the measurement region is at least partly surrounded by a shield constructed from high-conductivity material.

Example 5: The non-contact electric potential meter system of any of Examples 1-4, further comprising a flexible sensing attachment providing the measurement region, wherein the flexible sensing attachment in operation is configured to at least partly surround the first hot conductor.

Example 6: The non-contact electric potential meter system of any of Examples 1-5, wherein the flexible sensing attachment of Example 5 comprises the shield of Example 4.

Example 7: The non-contact electric potential meter system of any of Examples 1-6, wherein the flexible sensing attachment of Example 5 comprises a bi-stable structure, such as a bi-stable spring.

Example 8: The non-contact electric potential meter system of any of Examples 1-7, wherein the capacitance-determining electronic circuitry includes a shield driver circuit or chip.

Example 9: The non-contact electric potential meter system of any of Examples 1-8, wherein the shield driver circuit or chip of Example 8 drives the shield of Example 4 with a signal or waveform to reduce a measurement of a capacitance or of an induced displacement current between the shield and the electrode.

Example 10: The non-contact electric potential meter system of any of Examples 1-9, further comprising a multiplexing circuit configured to selectively couple the shield of Example 4 to the reference potential or to the shield driver circuit or chip of Example 8.

Example 11: The non-contact electric potential meter system of any of Examples 1-10, wherein the multiplexing circuit of Example 10 is configured to couple the shield to the reference potential when the waveform-sensing electronic circuitry is in operation, and to the shield driver circuit or chip of Example 8 to drive it to approximately the same potential as the electrode to minimize an effect or a measurement of a capacitance between them when the capacitance-determining electronic circuitry is in operation.

Example 12: The non-contact electric potential meter system of any of Examples 1-11, wherein the flexible sensing attachment of Example 5 is configured to wrap around the first hot conductor.



- Example 13: The non-contact electric potential meter system of any of Examples 1-12, wherein the flexible sensing attachment of Example 5 is configured to wrap around the first hot conductor to produce a determinable geometric relationship between the electrode and the first hot conductor, and wherein the determinable geometric relationship comprises a closest distance of between 1 mm and 15 mm. 5
- Example 14: The non-contact electric potential meter system of any of Examples 1-13, wherein the flexible sensing attachment of Example 5 includes a relatively more flexible portion and a relatively less flexible portion. 10
- Example 15: The non-contact electric potential meter system of any of Examples 1-14, further comprising a rigid portion and/or a housing. 15
- Example 16: The non-contact electric potential meter system of any of Examples 1-15, further comprising a housing or attachment configured to connect to or be grabbable by a "hot stick" tool. 20
- Example 17: The non-contact electric potential meter system of any of Examples 1-16, wherein the signal processing electronic circuitry is configured to process the AC voltage waveform obtained by the waveform-sensing electronic circuitry to obtain a line voltage waveform frequency spectrum or shape, and to scale the obtained line voltage waveform frequency spectrum or shape using the scaling factor based on the coupling capacitance obtained by the capacitance-determining electronic circuitry. 25 30
- Example 18: The non-contact electric potential meter system of any of Examples 1-17, wherein the waveform-sensing electronic circuitry configured to obtain an AC voltage waveform induced by capacitive coupling between the first hot conductor and the electrode comprises an amplifier circuit having an output that depends on the coupling capacitance formed between the first hot conductor and the electrode and depends on the voltage between the first hot conductor and the reference potential. 35 40
- Example 19: The non-contact electric potential meter system of any of Examples 1-18, wherein the amplifier circuit comprises a transimpedance amplifier circuit having an output that scales linearly with the coupling capacitance and with the voltage between the first hot conductor and the reference potential. 45
- Example 20: The non-contact electric potential meter system of any of Examples 1-19, wherein:  
the capacitance-determining electronic circuitry comprises coupling capacitance tracking circuitry configured to have an output frequency that depends on the coupling capacitance formed between the first hot conductor and the electrode; and  
the capacitance-determining electronic circuitry comprises scaling factor obtaining circuitry configured to obtain the scaling factor based on the output frequency of the coupling capacitance tracking circuitry. 50 55
- Example 21: The non-contact electric potential meter system of any of Examples 1-20, wherein the capacitance-determining electronic circuitry comprises a circuit including an astable op-amp multivibrator that is configured to switch an output signal between an output voltage and a ground potential at a switching frequency inversely proportional to the coupling capacitance formed between the first hot conductor and the electrode. 60 65

- Example 22: The non-contact electric potential meter system of any of Examples 1-21, wherein the capacitance-determining electronic circuitry includes a capacitance measurement chip or circuit.
- Example 23: The non-contact electric potential meter system of any of Examples 1-22, wherein the capacitance-determining electronic circuitry comprises a calibration circuit including a relaxation oscillator, a reference capacitance to the reference potential, a switch configured to selectively connect the reference capacitance and the coupling capacitance, and circuitry configured to obtain a difference between a first frequency of the calibration circuit when the switch is open, and a second frequency of the calibration circuit when the switch is closed.
- Example 24: The non-contact electric potential meter system of any of Examples 1-23, wherein the capacitive AC voltage sensing mechanism comprises:  
measurement means to obtain a determination of at least one physical dimension of the first hot conductor;  
electronic circuitry configured to obtain, based on the determination of the at least one physical dimension of the first hot conductor, a determination of a distance between the electrode and a center of the first hot conductor; and  
wherein the capacitance-determining electronic circuitry is configured to use the determined distance between the electrode and the center of the first hot conductor and the determined at least one physical characteristic of the first hot conductor to obtain the scaling factor based on the coupling capacitance formed between the first hot conductor and the electrode.
- Example 25: The non-contact electric potential meter system of any of Examples 1-24, wherein the measurement means of Example 24 are configured to sense one or more of: a diameter of the first hot conductor including an insulating layer, a circumference of the first hot conductor, a distance indicator of the flexible sensing attachment of Example 5, or a curvature or bending of the flexible sensing attachment of Example 5.
- Example 26: The non-contact electric potential meter system of any of Examples 1-25, further comprising:  
a current sensing mechanism, comprising:  
a current transformer configured to measure the current in the first hot conductor; and  
current processing electronic circuitry configured to obtain a determination of the current in the first hot conductor.
- Example 27: The non-contact electric potential meter system of any of Examples 1-26, wherein the signal processing electronic circuitry is configured to process and time-synchronize a current waveform and a voltage waveform of the first alternating current electrical circuit to obtain a determination of a power factor of the first alternating current electrical circuit.
- Example 28: The non-contact electric potential meter system of any of Examples 1-27, further comprising power supply means configured to power the electronic circuitry.
- Example 29: The non-contact electric potential meter system of any of Examples 1-28, wherein the power supply means of Example 28 comprise one or more of a stored energy system such as a capacitor or battery, an external power supply such as a DC voltage source, or



31

energy harvesting circuitry suitable for obtaining power from the first alternating current electrical circuit.

Example 30: The non-contact electric potential meter system of any of Examples 1-29, further comprising a multiplexing circuit configured to share a current transformer between a current sensing mechanism and the energy harvesting circuitry.

Example 31: The non-contact electric potential meter system of any of Examples 1-30, further comprising a multiplexing circuit configured to selectively couple the electrode to the waveform-sensing electronic circuitry or to the capacitance-determining electronic circuitry.

What is claimed is:

1. A non-contact electric potential meter system suitable for obtaining a determination of a voltage between a first hot conductor of a first alternating current (AC) electrical circuit and a reference potential, without direct electrical contact to the first hot conductor and without comparison to a second AC voltage signal, the non-contact electric potential meter system comprising:

a measurement region configured to receive the first hot conductor without interruption of the first hot conductor; and

a capacitive AC voltage sensing mechanism, comprising: an electrode situated near the first hot conductor when the measurement region has received the first hot conductor;

wherein the electrode includes a conductive layer affixed to or formed in or by a flexible PCB or other flexible substrate;

waveform-sensing electronic circuitry configured to obtain an AC voltage waveform induced by capacitive coupling between the first hot conductor and the electrode;

capacitance-determining electronic circuitry configured to obtain a scaling factor based on a coupling capacitance formed between the first hot conductor and the electrode; and

signal processing electronic circuitry configured to obtain, from the AC voltage waveform obtained by the waveform-sensing electronic circuitry and the coupling capacitance-based scaling factor obtained by the capacitance-determining electronic circuitry, the voltage between the first hot conductor and the reference potential.

2. The non-contact electric potential meter system of claim 1, wherein the measurement region is configured such that no other conductor is received by the measurement region.

3. The non-contact electric potential meter system of claim 1, wherein the measurement region is at least partly surrounded by a shield constructed from high-conductivity material.

4. The non-contact electric potential meter system of claim 1, further comprising a rigid portion and/or a housing.

5. The non-contact electric potential meter system of claim 1, further comprising a housing or attachment configured to connect to or be grabbable by a "hot stick" tool.

6. The non-contact electric potential meter system of claim 1, wherein the signal processing electronic circuitry is configured to process the AC voltage waveform obtained by the waveform-sensing electronic circuitry to obtain a line voltage waveform frequency spectrum or shape, and to scale the obtained line voltage waveform frequency spectrum or

32

shape using the scaling factor based on the coupling capacitance obtained by the capacitance-determining electronic circuitry.

7. The non-contact electric potential meter system of claim 1, wherein the waveform-sensing electronic circuitry configured to obtain an AC voltage waveform induced by capacitive coupling between the first hot conductor and the electrode comprises an amplifier circuit having an output that depends on the coupling capacitance formed between the first hot conductor and the electrode and depends on the voltage between the first hot conductor and the reference potential.

8. The non-contact electric potential meter system of claim 7, wherein the amplifier circuit comprises a transimpedance amplifier circuit having an output that scales linearly with the coupling capacitance and with the voltage between the first hot conductor and the reference potential.

9. The non-contact electric potential meter system of claim 1, wherein:

the capacitance-determining electronic circuitry comprises coupling capacitance tracking circuitry configured to have an output frequency that depends on the coupling capacitance formed between the first hot conductor and the electrode; and

the capacitance-determining electronic circuitry comprises scaling factor obtaining circuitry configured to obtain the scaling factor based on the output frequency of the coupling capacitance tracking circuitry.

10. The non-contact electric potential meter system of claim 1, wherein the capacitance-determining electronic circuitry comprises a circuit including an astable op-amp multivibrator that is configured to switch an output signal between an output voltage and a ground potential at a switching frequency inversely proportional to the coupling capacitance formed between the first hot conductor and the electrode.

11. The non-contact electric potential meter system of claim 1, wherein the capacitance-determining electronic circuitry comprises a calibration circuit including a relaxation oscillator, a reference capacitance to the reference potential, a switch configured to selectively connect the reference capacitance and the coupling capacitance, and circuitry configured to obtain a difference between a first frequency of the calibration circuit when the switch is open, and a second frequency of the calibration circuit when the switch is closed.

12. The non-contact electric potential meter system of claim 1, wherein the capacitive AC voltage sensing mechanism comprises:

measurement means to obtain a determination of at least one physical dimension or characteristic of the first hot conductor;

electronic circuitry configured to obtain, based on the determination of the at least one physical dimension or characteristic of the first hot conductor, a determination of a distance between the electrode and a center of the first hot conductor; and

wherein the capacitance-determining electronic circuitry is configured to use the determined distance between the electrode and the center of the first hot conductor and the determined at least one physical dimension or characteristic of the first hot conductor to obtain the scaling factor based on the coupling capacitance formed between the first hot conductor and the electrode.

13. The non-contact electric potential meter system of claim 12, wherein the measurement means are configured to



33

sense one or more of: a diameter of the first hot conductor including an insulating layer, a circumference of the first hot conductor, a distance indicator of a flexible sensing attachment, or a curvature or bending of the flexible sensing attachment.

14. The non-contact electric potential meter system of claim 1, further comprising:

a current sensing mechanism, comprising:

a current transformer configured to measure the current in the first hot conductor; and

current processing electronic circuitry configured to obtain a determination of the current in the first hot conductor.

15. The non-contact electric potential meter system of claim 1, wherein the signal processing electronic circuitry is configured to process and time-synchronize a current waveform and a voltage waveform of the first alternating current electrical circuit to obtain a determination of a power factor of the first alternating current electrical circuit.

16. The non-contact electric potential meter system of claim 1, further comprising power supply means configured to power the electronic circuitry.

17. The non-contact electric potential meter system of claim 16, wherein the power supply means comprise one or more of a stored energy system, an external power supply, or energy harvesting circuitry suitable for obtaining power from the first alternating current electrical circuit.

18. The non-contact electric potential meter system of claim 1, further comprising a multiplexing circuit configured to share a current transformer between a current sensing mechanism and the energy harvesting circuitry, or configured to selectively couple the electrode to the waveform-sensing electronic circuitry or to the capacitance-determining electronic circuitry.

19. The non-contact electric potential meter system of claim 1, wherein the capacitance-determining electronic circuitry includes a capacitance measurement chip or circuit.

20. A non-contact electric potential meter system suitable for obtaining a determination of a voltage between a first hot conductor of a first alternating current (AC) electrical circuit and a reference potential, without direct electrical contact to the first hot conductor and without comparison to a second AC voltage signal, the non-contact electric potential meter system comprising:

a flexible sensing attachment providing a measurement region configured to receive the first hot conductor without interruption of the first hot conductor, wherein the flexible sensing attachment in operation is configured to at least partly surround the first hot conductor; and

a capacitive AC voltage sensing mechanism, comprising: an electrode situated near the first hot conductor when the measurement region has received the first hot conductor;

waveform-sensing electronic circuitry configured to obtain an AC voltage waveform induced by capacitive coupling between the first hot conductor and the electrode;

capacitance-determining electronic circuitry configured to obtain a scaling factor based on a coupling capacitance formed between the first hot conductor and the electrode; and

signal processing electronic circuitry configured to obtain, from the AC voltage waveform obtained by the waveform-sensing electronic circuitry and the coupling capacitance-based scaling factor obtained

34

by the capacitance-determining electronic circuitry, the voltage between the first hot conductor and the reference potential.

21. The non-contact electric potential meter system of claim 20, wherein the flexible sensing attachment comprises a shield constructed from high-conductivity material.

22. The non-contact electric potential meter system of claim 20, wherein the flexible sensing attachment comprises a bi-stable structure.

23. The non-contact electric potential meter system of claim 20, wherein the flexible sensing attachment is configured to wrap around the first hot conductor.

24. The non-contact electric potential meter system of claim 20, wherein the flexible sensing attachment is configured to wrap around the first hot conductor to produce a determinable geometric relationship between the electrode and the first hot conductor, and wherein the determinable geometric relationship comprises a closest distance of between 1 mm and 15 mm.

25. The non-contact electric potential meter system of claim 20, wherein the flexible sensing attachment includes a relatively more flexible portion and a relatively less flexible portion.

26. A non-contact electric potential meter system suitable for obtaining a determination of a voltage between a first hot conductor of a first alternating current (AC) electrical circuit and a reference potential, without direct electrical contact to the first hot conductor and without comparison to a second AC voltage signal, the non-contact electric potential meter system comprising:

a measurement region configured to receive the first hot conductor without interruption of the first hot conductor; and

a capacitive AC voltage sensing mechanism, comprising: an electrode situated near the first hot conductor when the measurement region has received the first hot conductor;

waveform-sensing electronic circuitry configured to obtain an AC voltage waveform induced by capacitive coupling between the first hot conductor and the electrode;

capacitance-determining electronic circuitry configured to obtain a scaling factor based on a coupling capacitance formed between the first hot conductor and the electrode;

wherein the capacitance-determining electronic circuitry includes a shield driver for driving a shield constructed from high-conductivity material; and signal processing electronic circuitry configured to obtain, from the AC voltage waveform obtained by the waveform-sensing electronic circuitry and the coupling capacitance-based scaling factor obtained by the capacitance-determining electronic circuitry, the voltage between the first hot conductor and the reference potential.

27. The non-contact electric potential meter system of claim 26, wherein the shield driver drives the shield with a signal or waveform to reduce a measurement of a capacitance or of an induced displacement current between the shield and the electrode.

28. The non-contact electric potential meter system of claim 26, further comprising a multiplexing circuit configured to selectively couple the shield to the reference potential or to the shield driver.

29. The non-contact electric potential meter system of claim 28, wherein the multiplexing circuit is configured to couple the shield to the reference potential when the wave-



form-sensing electronic circuitry is in operation, and to the shield driver to drive it to approximately the same potential as the electrode to minimize an effect or a measurement of a capacitance between them when the capacitance-determining electronic circuitry is in operation.

5

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